

Full Length Research Paper

Probabilistic analysis of two warm standby system with instructions at need

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This paper is concerned with two unit warm standby systems having one expert repairman and one assistant repairman. The assistant is called only if the expert repairman is busy. The assistant repairman who may repair the failed unit after getting instructions by his master; but sometimes the assistant repairman may repair it without having the need of instructions for doing repair with probability p and q , respectively. Techniques of the semi-Markov processes and regenerative processes are used to obtain various measures of system effectiveness mean time to system failure (MTSF), availability analysis, busy period of an expert repairman, busy period of an assistant repairman and profit incurred.

Key words: Mean time to system failure (MTSF), availability, warm standby.

INTRODUCTION

In reliability analysis of redundant repairable systems, most of the research workers have concentrated their attention on cold standby systems, and have emphasized the importance of warm standby (Goel et al., 1985; Kumar et al., 1995; Pour and Singh, 1996; Sridharan and Mohanavadivu, 1998; Singh et al., 2000). And in most of these papers one of the basic assumptions is that only one repairman facility (Kuo-Hsiung and Wen-Lea, 2006; Labib, 1991; Mokaddis et al., 2009a; 2009b). However, it may not be true in all situations. There may be situations when we should call two repairmen who may do the job at the same time. So when an expert repairman is busy for repairing a failed unit and another unit fails. Then the assistant repairman who may repair the failed unit after getting instructions by his master; but sometimes the assistant repairman may repair it without having the need of instructions because the faults in the failed unit are minor. Thus, in this paper, a two-unit warm standby system is studied incorporating the above idea, with some usual assumptions and the following additional assumptions:

- (i) The system consists of two identical units. Initially one unit is operative and the other unit is warm standby,
- (ii) When failure of a unit is detected and is attended by the expert repairman,
- (iii) System is down when both units are fail,
- (iv) When the expert repairman is called on to do his job, it takes negligible time to reach the system,
- (v) The expert repairman leaves the system after completing repair the failed unit. The other unit which fails will be attended to by the assistant repairman,
- (vi) After repair, the unit work as good as new,
- (viii) There is a single repair facility attended by the two repairmen (expert and assistant).

NOTATION

λ : Constant failure rate of the operative unit.
 μ : Constant failure rate of the standby unit.
 $W(t), w(t)$: Cdf and pdf of time to repair of failure standby.
 $G(t), g(t)$: Cdf and pdf of time to repair by expert repairman.
 $I(t), i(t)$: Cdf and pdf of time to when expert gives instructions.

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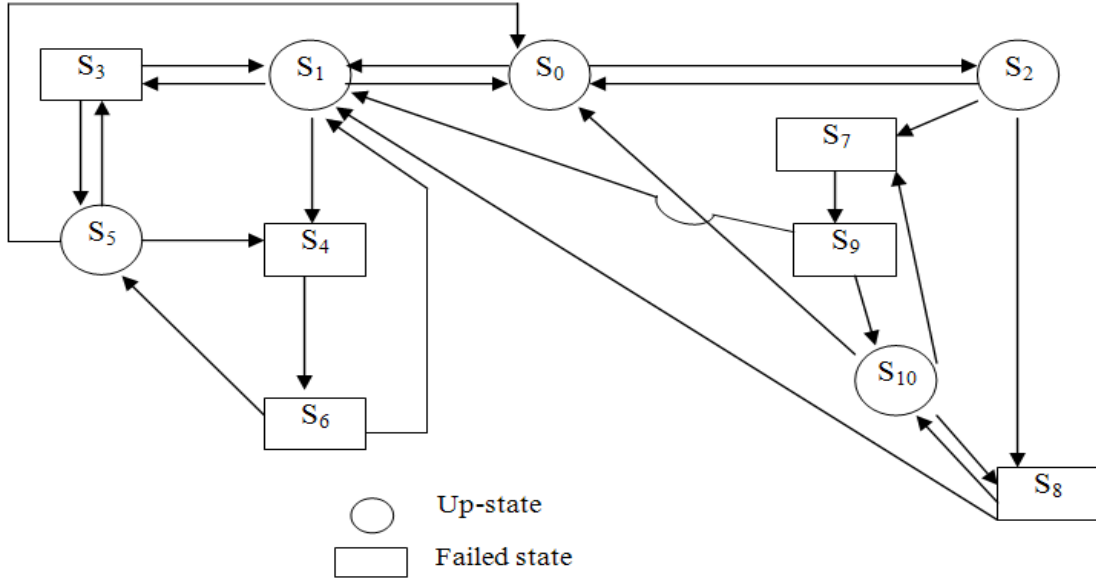


Figure 1. State transition diagram.

$U(t), u(t)$: Cdf and pdf of time to repair by to his assistance.

p/q : Probability that the assistant repairman needs/ does not need instructions before starting the repair.

p_{ij} : One step transition probability from state i to state j .

p_{ij}^k : Probability that the system in state i goes to state j through state k ; $i, j \in E$ and $k \in \bar{E}$.

E_0 : State of the system at epoch $t = 0$.

E : Set of regenerative states $\{S_0, S_1, S_2, S_4, S_5, S_6, S_7, S_9, S_{10}\}$.

\bar{E} : State of non regenerative states $\{S_3, S_8\}$.

$S_5(O, R_e)$: One unite is operative and the standby unit continuous to repair by expert repairman.

$S_6(r_e, r_a)$: One unit is under repair by the expert repairman and the other unit under repair by the assistant repairman.

$S_7(SW_{re}, W_m)$: One unit waiting for expert repairman and other unit waiting for assistant repairman.

$S_8(SR_e, r_a)$: One unit continuous to repair by expert repairman and the other unite under assistant repairman.

$S_9(Sr_e, r_a)$: One unit is under repair by the expert repairman and the other unit under repair by the assistant repairman.

$S_{10}(O, SR_e)$: One unite is operative and the standby unit continuous to repair by expert repairman.

TRANSITION PROBABILITIES AND SOJOURN TIMES

The system can take one of the following states (Figure 1):

$S_0(O, ST)$: One unit is operative and the other unit is kept as warm standby.

$S_1(r_e, O)$: One unit is operative and the other is under expert repairman.

$S_2(S_{re}, O)$: One unit is operative and warm standby unit under repair by the expert repairman.

$S_3(R_e, r_a)$: One unit continuous to repair by expert repairman and the other unite under assistant repairman.

$S_4(W_{re}, W_m)$: One unit waiting for expert repairman and other unit waiting for assistant repairman.

Mean time to system failure

Time to system failure can be regarded as the first passage to any of the failed states $S_3, S_4, S_6, S_7,$

S_8, S_9, S_{10} which is considered as absorbing.

Employing the arguments used for regenerative process the following recursive relations for $\tilde{\pi}_i(t)$ are obtained when $E_0=S_i$

$$\pi_0(t) = Q_{01} \pi_1(t) + Q_{02} \pi_2$$

$$\pi_1(t) = Q_{10} \pi_0(t) + Q_{13} + Q_{14}$$

$$\pi_2(t) = Q_{20} \pi_0(t) + Q_{27} + Q_{28}$$

$$\pi_5(t) = Q_{50} \pi_0(t) + Q_{53} + Q_{54}$$

$$\pi_{10}(t) = Q_{100} \pi_0(t) + Q_{107} + Q_{108}$$

Taking Laplace-Stieltjes transform for this equations and solving for $\tilde{\pi}_0(s)$ we get the mean time to system failure (MTSF) which is given by:

$$\frac{-d}{ds} \tilde{\pi}_0(s) \Big|_{s=0} = \frac{Q'_1(s) \tilde{N}_1(s)}{D_1(s)}$$

Where,

$$MTSF = \frac{\mu_0 + P_{01}\mu_1 + P_{02}\mu_2}{1 - P_{01}P_{10} + P_{02}P_{20}}$$

AVAILABILITY ANALYSIS

The following probabilistic arguments

$$\begin{aligned} \mu_0(t) &= \bar{F}(t)\bar{R}(t) & \mu_1(t) &= p\bar{F}(t)q\bar{F}(t)G(t) \\ \mu_2(t) &= p\bar{F}(t)q\bar{F}(t)\bar{W}(t) & \mu_5(t) &= p\bar{F}(t)q\bar{F}(t)\bar{W}(t) \\ \mu_{10}(t) &= p\bar{F}(t)q\bar{F}(t)\bar{W}(t) \end{aligned}$$

Can be used in the theory of regenerative process in order to find the point wise availabilities $A_i(t)$ as shown in following recessive relations:

$$\begin{aligned} A_0(t) &= M_0 t + Q_{01}(t) \odot A_1(t) + Q_{02}(t) \odot A_2(t) \\ A_1(t) &= M_1 t + Q_{10}(t) \odot A_0(t) + Q_{11}^3(t) \odot A_1(t) + Q_{15}^3(t) \odot A_5(t) + Q_{14} \odot A_4(t) \\ A_2(t) &= M_2 t + Q_{20}(t) \odot A_0(t) + Q_{27}(t) \odot A_7(t) + Q_{210}^8(t) \odot A_{10}(t) + Q_{21}^8(t) \odot A_1(t) \\ A_4(t) &= Q_{46}(t) \odot A_6(t) \\ A_5(t) &= M_5 t + Q_{50}(t) \odot A_0(t) + Q_{54}(t) \odot A_4(t) + Q_{55}^3(t) \odot A_5(t) + Q_{51}^3(t) \odot A_1(t) \\ A_6(t) &= Q_{61}(t) \odot A_1(t) + Q_{65}(t) \odot A_5(t) \\ A_7(t) &= Q_{79}(t) \odot A_9(t) \\ A_9(t) &= Q_{910}(t) \odot A_{10}(t) + Q_{91}(t) \odot A_1(t) \\ A_{10}(t) &= M_{10} t + Q_{100}(t) \odot A_0(t) + Q_{107}(t) \odot A_7(t) + Q_{1010}^8(t) \odot A_{10}(t) + Q_{101}^8(t) \odot A_1(t). \end{aligned}$$

After using Laplace transform for equations and solving for $A_0^*(s)$ we can calculate the steady state availability such that:

$$A_0 = \lim_{s \rightarrow 0} sA_0^*(s) = \frac{N_2(0)}{D_2'(0)}$$

Where,

$$\begin{aligned} D_2'(0) &= \mu_0 (1 - P_{107}P_{79}P_{910} - P_{1010}^8 - P_{50} - P_{14}P_{46}P_{65} \\ &+ P_{15}^3 + P_{10}(1 - P_{46}P_{54}P_{65} - P_{55}^3)) \\ &+ \mu_1 (P_{01} (1 - P_{107}P_{79}P_{910} - P_{1010}^8) + P_{02} (P_{27}P_{79} \\ &(P_{910}P_{101}^8 + P_{91}(1 - P_{1010}^8)) + (1 - P_{107}P_{79}P_{910} \\ &- P_{1010}^8)P_{21}^8 + (P_{107}P_{79}P_{91} + P_{101}^8) P_{210}^8)) \\ &(1 - P_{46}P_{54}P_{65} - P_{55}^3) \\ &+ \mu_2 P_{02} (1 + P_{107}P_{79}P_{910} + P_{1010}^8) + (P_{50} (P_{14}P_{46}P_{65} \\ &+ P_{15}^3) + P_{10} (1 - P_{46}P_{54}P_{65}P_{55}^3) \\ &+ \mu_4 (P_{54} - P_{61}P_{15}^3 - 1 - P_{107}P_{79}P_{910} - P_{1010}^8 - P_{02} - P_{20} \\ &1 - P_{107}P_{79}P_{910} - P_{1010}^8 + P_{100} - P_{27}P_{79}P_{910} + P_{210}^8 \\ &+ P_{65} - 1 - P_{107}P_{79}P_{910} - P_{1010}^8 - 1 - P_{11}^3 - P_{01}P_{10} \\ &1 - P_{107}P_{79}P_{910} - P_{1010}^8 - P_{100} - 1 - P_{11}^3 \\ &P_{27}P_{79}P_{910} + P_{210}^8 - P_{10} - P_{27}P_{79} - P_{91} + P_{910} + P_{1010}^8 \\ &P_{21}^8 + P_{107}P_{79}P_{91} + P_{101}^8 - P_{210}^8 + P_{14} \\ &P_{65}P_{65} - P_{01}P_{50} - 1 + P_{1010}^8 + P_{107}P_{79}P_{910} - 1 \\ &- P_{107}P_{79}P_{910} - P_{1010}^8 - P_{51}^3 + P_{02} - P_{50} \\ &P_{21}^8 - 1 - P_{107}P_{79}P_{910} - P_{1010}^8 + P_{107}P_{79}P_{91} + P_{101}^8 \\ &P_{210}^8 - P_{20} - 1 - P_{107}P_{79}P_{910} - P_{1010}^8 - P_{100}P_{210}^8 - P_{51}^3 \\ &+ P_{27}P_{79} - P_{50} - P_{910}P_{101}^8 + P_{91} - 1 - P_{1010}^8 \\ &- P_{100}P_{910}P_{51}^3 + P_{61} - 1 - P_{107}P_{79}P_{910} - P_{1010}^8 - P_{02} \\ &P_{20} - 1 - P_{107}P_{79}P_{910} - P_{1010}^8 + P_{100} - P_{27}P_{79}P_{910} + P_{210}^8 - 1 - P_{55}^3 \\ &+ \mu_5 (P_{14}P_{46}P_{65} + P_{15}^3 - 1 - P_{107}P_{79}P_{910} - P_{1010}^8 - P_{02} \\ &P_{20} - 1 - P_{1010}^8 - P_{107}P_{79}P_{910} + P_{100} - P_{107}P_{79}P_{910} \\ &+ P_{210}^8 \\ &+ \mu_6 P_{46} - 1 - P_{107}P_{79}P_{910} - P_{1010}^8 - P_{02} - P_{20} - 1 \\ &- P_{107}P_{79}P_{910} - P_{1010}^8 + P_{100} - P_{107}P_{79}P_{910} + P_{210}^8 \\ &P_{54}P_{15}^3 + P_{14} - 1 - P_{55}^3 \\ &+ \mu_7 (P_{107} - P_{910} - 1 - P_{01}P_{10} - P_{02}P_{20} - P_{11}^3 - 1 \\ &- P_{02}P_{20} - P_{02}P_{10}P_{21}^8 - 1 - P_{46}P_{54}P_{65} - P_{55}^3 - P_{14}P_{46} \\ &1 - P_{02}P_{20} - P_{61} - 1 - P_{55}^3 + P_{65}P_{51}^3 - P_{01}P_{50} \end{aligned}$$

$$\begin{aligned}
 &+P_{02}P_{50}P_{21}^8 + P_{51}^3 (1 - P_{02}P_{20} P_{46}P_{54}P_{65} + P_{15}^3) \\
 &+P_{02}P_{210}^8P_{91} P_{10} (1 - P_{46}P_{54}P_{65} - P_{55}^3) + P_{50} P_{15}^3 \\
 &+P_{14}P_{46}P_{65} + P_{02}P_{27} \\
 &P_{91}P_{10} (1 - P_{46}P_{54}P_{65} + P_{14}P_{46}P_{50}P_{65} + P_{910}P_{100} (1 \\
 &-P_{46}P_{54}P_{65} - P_{14}P_{46}P_{61} - P_{11}^3) + P_{55}^3) (1 \\
 &-P_{46}P_{54}P_{65} - P_{11}^3P_{55}^3 - P_{15}^3 P_{51}^3) + P_{14}P_{46}P_{65} \\
 &+P_{46}P_{54}P_{61} P_{91} (1 - P_{1010}^8) + P_{910}P_{101}^8 \\
 &P_{50}P_{15}^3 - P_{10}P_{55}^8 + \mu_9P_{02}P_{79} (P_{27} (1 - P_{1010}^8) \\
 &+ P_{107}P_{210}^8) (P_{50} (P_{14}P_{46}P_{65} + P_{15}^3) \\
 &+ P_{10} (1 - P_{46}P_{54}P_{65} - P_{55}^3)) + \mu_{10}P_{02} (P_{27}P_{79}P_{910} \\
 &+ P_{210}^8) (P_{50} (P_{14}P_{46}P_{65} + P_{15}^3) + P_{10} (1 - P_{46}P_{54}P_{65} \\
 &- P_{55}^3)) \\
 N_2(0) &= Y_0 + Y_1 + Y_2 + Y_5 + Y_{10}
 \end{aligned}$$

$$\begin{aligned}
 Y_0 &= \mu_0 [(1 - P_{107}P_{79}P_{910} - P_{1010}^8) (1 - P_{11}^3 - P_{46}P_{54} \\
 &(P_{65} (1 - P_{11}^3) + P_{61}P_{15}^3) - P_{15}^3P_{51}^3 - P_{14}P_{46} (P_{65}P_{51}^3 \\
 &- P_{61} (1 - P_{55}^3)) - P_{55}^3 + P_{11}^3P_{55}^3)]
 \end{aligned}$$

$$\begin{aligned}
 Y_1 &= \mu_1 [(1 - P_{46}P_{54}P_{65} - P_{55}^3) (P_{01} (1 - P_{107}P_{79}P_{910} \\
 &- P_{1010}^8) - P_{02} (P_{27}P_{79} (P_{910}P_{101}^8 + P_{91} (1 - P_{1010}^8)) \\
 &+ P_{21}^8(1 - P_{107}P_{79}P_{910} - P_{1010}^8) + P_{210}^8 (P_{107}P_{79}P_{91} \\
 &+ P_{101}^8)))]
 \end{aligned}$$

$$\begin{aligned}
 Y_2 &= \mu_2P_{02} [(1 - P_{107}P_{79}P_{910} - P_{1010}^8) (1 - P_{11}^3 - P_{46}P_{54} \\
 &(P_{65} (1 - P_{11}^3) + P_{61}P_{15}^3) - P_{15}^3P_{51}^3 - P_{14}P_{46} (P_{65}P_{51}^3 \\
 &+ P_{61} (1 - P_{55}^3)) + P_{55}^3 - P_{11}^3P_{55}^3)]
 \end{aligned}$$

$$\begin{aligned}
 Y_5 &= \mu_5 [(P_{14}P_{46}P_{65} + P_{15}^3) (P_{01} (1 - P_{107}P_{79}P_{910} - P_{1010}^8) \\
 &+ P_{02} (P_{27}P_{79} (P_{910}P_{101}^8 + P_{91} (1 - P_{1010}^8)) + P_{21}^8(1 \\
 &- P_{107}P_{79}P_{910} - P_{1010}^8) + P_{210}^8 (P_{107}P_{79}P_{91} + P_{101}^8)))]
 \end{aligned}$$

$$\begin{aligned}
 Y_{10} &= \mu_{10} [P_{02} (P_{27}P_{79}P_{910} + P_{210}^8) (1 - P_{11}^3 - P_{46}P_{54} \\
 &(P_{65} (1 - P_{11}^3) - P_{61}P_{15}^3) - P_{15}^3P_{51}^3 - P_{14}P_{46} \\
 &(P_{65}P_{15}^3 + P_{61} (1 - P_{55}^3)) - P_{55}^3 + P_{11}^3P_{55}^3)]
 \end{aligned}$$

BUSY PERIOD OF AN EXPERT REPAIRMAN

The following probabilistic arguments

$$\begin{aligned}
 \mu_0(t) &= \bar{F}(t)\bar{R}(t) & \mu_1(t) &= p\bar{F}(t)q\bar{F}(t)G(t) \\
 \mu_2(t) &= p\bar{F}(t)q\bar{F}(t)\bar{W}(t) & \mu_5(t) &= p\bar{F}(t)q\bar{F}(t)\bar{W}(t) \\
 \mu_{10}(t) &= p\bar{F}(t)q\bar{F}(t)\bar{W}(t)
 \end{aligned}$$

Can be used in the theory of regenerative process in order to find the busy period analysis for the expert repairman $B_i(t)$ (the probability that the operative unit is under repair at time (t) as shown in following recessive relations:

$$\begin{aligned}
 B_0(t) &= Q_{01}(t) B_1(t) + Q_{02}(t) B_2(t) \\
 B_1(t) &= W_1(t) + Q_{10}(t) B_0(t) + Q_{11}^3(t) B_1(t) + Q_{15}^3(t) B_5(t) + Q_{14}(t) B_4(t) \\
 B_2(t) &= W_2(t) + Q_{20}(t) B_0(t) + Q_{27}(t) B_7(t) + Q_{2,10}^8(t) B_{10}(t) + Q_{21}^8(t) B_1(t) \\
 B_4(t) &= W_4(t) + Q_{46}(t) B_6(t) \\
 B_5(t) &= W_5(t) + Q_{50}(t) B_0(t) + Q_{54}(t) B_4(t) + Q_{55}^3(t) B_5(t) + Q_{51}^3(t) B_1(t) \\
 B_6(t) &= W_6(t) + Q_{61}(t) B_1(t) + Q_{65}(t) B_5(t) \\
 B_7(t) &= W_7(t) + Q_{79}(t) B_9(t) \\
 B_8(t) &= W_9(t) + Q_{9,10}(t) B_{10}(t) + Q_{9,1}(t) B_1(t) \\
 B_{10}(t) &= W_{10}(t) + Q_{10,0}(t)B_0(t) + Q_{10,7}(t)B_7(t) + Q_{10,10}^8(t)B_{10}(t) + Q_{10,1}^8(t)B_1(t).
 \end{aligned}$$

After using Laplace transform for equations and solving for $B_0^*(s)$ we can calculate the busy period analysis steady such that:

$$B_0 = \lim_{s \rightarrow 0} s\tilde{B}_0(s) = \frac{N_3(0)}{D_2'(0)}$$

Where,

$$N_3(0) = Y_1 + Y_2 + Y_4 + Y_5 + Y_6 + Y_7$$

$$\begin{aligned}
 Y_1 &= \mu_1 [(1 - P_{46}P_{54}P_{65} - P_{55}^3) (P_{01} (1 - P_{107}P_{79}P_{910} \\
 &- P_{1010}^8) - P_{02} (P_{27}P_{79} (P_{910}P_{101}^8 + P_{91} (1 - P_{1010}^8)) \\
 &+ P_{21}^8(1 - P_{107}P_{79}P_{910} - P_{1010}^8) + P_{210}^8 (P_{107}P_{79}P_{91} \\
 &+ P_{101}^8)))]
 \end{aligned}$$

$$\begin{aligned}
 Y_2 &= \mu_2P_{02} [(1 - P_{107}P_{79}P_{910} - P_{1010}^8) (1 - P_{11}^3 - P_{46}P_{54} (P_{65} \\
 &(1 - P_{11}^3) + P_{61}P_{15}^3) - P_{15}^3P_{51}^3 - P_{14}P_{46} (P_{65}P_{51}^3 + P_{61} (1 - P_{55}^3)) \\
 &+ P_{55}^3 - P_{11}^3P_{55}^3)] \\
 Y_4 &= \mu_4 [(P_{01} (1 - P_{107}P_{79}P_{910} - P_{1010}^8) + P_{02} (P_{27}P_{79} \\
 &(P_{910}P_{101}^8 + P_{91} (1 - P_{1010}^8)) + P_{21}^8 (1 - P_{107}P_{79}P_{910} \\
 &- P_{1010}^8) + P_{210}^8 (P_{107}P_{79}P_{91} + P_{101}^8)))] (P_{54}P_{15}^3 \\
 &+ P_{14}(1 - P_{55}^3))
 \end{aligned}$$

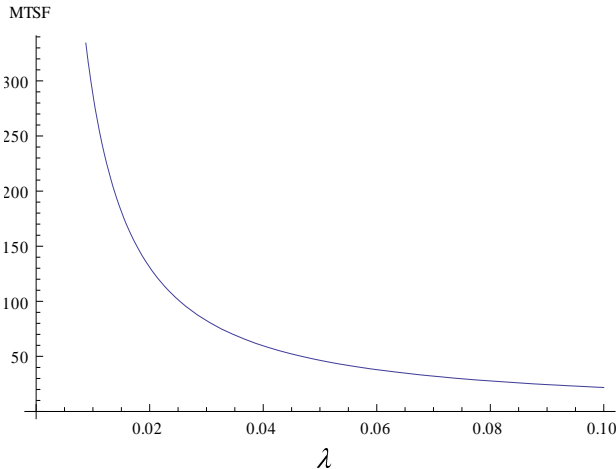


Figure 2. MTSF versus failure rate λ .

$$Y_6 = \mu_6 [p_{46} (p_{01} (1 - p_{107}p_{79}p_{910} - p_{1010}^8) + p_{02} (p_{27}p_{79} (p_{910}p_{101}^8 + p_{91} (1 - p_{1010}^8)) + p_{21}^8 (1 - p_{107}p_{79}p_{910} - p_{1010}^8) - p_{210}^8 (p_{107}p_{79}p_{91} + p_{101}^8))) (p_{54}p_{15}^3 + p_{14}(1 - p_{55}^3))]$$

$$Y_7 = \mu_7 [p_{02} (p_{27} (1 - p_{1010}^8) + p_{107}p_{210}^8) (1 - p_{11}^3 - p_{46}p_{54} (p_{65} (1 - p_{11}^3) + p_{61}p_{15}^3) - p_{15}^3p_{51}^3 - p_{14}p_{46} (p_{65}p_{51}^3 + p_{61} (1 - p_{55}^3)) - p_{55}^3 + p_{11}^3p_{55}^3)]]$$

$$Y_9 = \mu_9 [p_{02}p_{79} (p_{27} (1 - p_{1010}^8) + p_{107}p_{210}^8) (1 - p_{11}^3 - p_{46}p_{54} (p_{65} (1 - p_{11}^3) - p_{61}p_{15}^3p_{51}^3 - p_{14}p_{46} (p_{65}p_{51}^3 - p_{61} (1 - p_{55}^3)) - p_{55}^3 + p_{11}^3p_{55}^3)]]$$

BUSY PERIOD OF AN ASSISTANT REPAIRMAN

The following probabilistic arguments,

$$\begin{aligned} \mu_0(t) &= \bar{F}(t)\bar{R}(t) & \mu_4(t) &= p\bar{F}(t)q\bar{F}(t)G(t) \\ \mu_2(t) &= p\bar{F}(t)q\bar{F}(t)\bar{W}(t) & \mu_5(t) &= p\bar{F}(t)q\bar{F}(t)\bar{W}(t) \\ \mu_{10}(t) &= p\bar{F}(t)q\bar{F}(t)\bar{W}(t) \end{aligned}$$

Can be used in the theory of regenerative process in order to find the busy period analysis $T_i(t)$ (the probability that the operative unit is under repair at time (t) as shown in following recessive relations:

$$\begin{aligned} T_0(t) &= Q_{01}(t) & T_1(t) &= Q_{02}(t) & T_2(t) \\ T_1(t) &= Q_{10}(t) & T_0(t) &+ Q_{11}^3(t) & T_1(t) &+ Q_{15}^3(t) & T_5(t) &+ Q_{14}(t) & T_4(t) \end{aligned}$$

$$\begin{aligned} T_2(t) &= Q_{20}(t) & T_0(t) &+ Q_{27}(t) & T_7(t) &+ Q_{2,10}^8(t) & T_{10}(t) &+ Q_{21}^8(t) & T_1(t) \\ T_4(t) &= W_4(t) &+ Q_{46}(t) & & T_6(t) \\ T_5(t) &= Q_{50}(t) & T_0(t) &+ Q_{54}(t) & T_4(t) &+ Q_{55}^3(t) & T_5(t) &+ Q_{51}^3(t) & T_1(t) \\ T_6(t) &= W_6(t) &+ Q_{61}(t) & & T_1(t) &+ Q_{65}(t) & T_5(t) \\ T_7(t) &= W_7(t) &+ Q_{79}(t) & & T_9(t) \\ T_8(t) &= W_8(t) &+ Q_{9,10}(t) & & T_{10}(t) &+ Q_{9,1}(t) & T_1(t) \\ T_{10}(t) &= Q_{10,0}(t) & T_0(t) &+ Q_{10,7}(t) & T_7(t) &+ Q_{10,10}^8(t) & T_{10}(t) &+ Q_{10,1}^8(t) & T_1(t) \end{aligned}$$

After using Laplace transform for equations and solving for $T_0^*(s)$ we can calculate the busy period analysis steady such that:

$$T_0 = \lim_{s \rightarrow 0} s \tilde{T}_0^*(s) = \frac{N_4(0)}{D_2'(0)}$$

Where,

$$N_2(0) = Y_4 + Y_6 + Y_7 + Y_9$$

COST BENEFIT ANALYSIS

At steady state the net expected gain per unit of time is:

$$G = \lim_{t \rightarrow \infty} G(t)/t = C_1A_0 - C_2B_0 - C_3T_0,$$

Where,

- C_1 : Is revenue per unit uptime by the system.
- C_2 : Is per unit expert repair cost.
- C_3 : Is per unit assistant repair cost.

SPECIAL CASES

The failure and repair times are exponential distribution

$$\begin{aligned} F(t) &= 1 - e^{-\lambda t}, & I(t) &= 1 - e^{-\tau t}, \\ G(t) &= 1 - e^{-\alpha t}, & X(t) &= 1 - e^{-\nu t}, \\ U(t) &= 1 - e^{-\beta t}, & W(t) &= 1 - e^{-\theta t}. \end{aligned}$$

Graphical representation

The graphical representations are shown in Figures 2, 3 and 4.

Conclusion

By comparing the characteristic, MTSF, Availability and PROFIT with respect to λ , it was observing that:

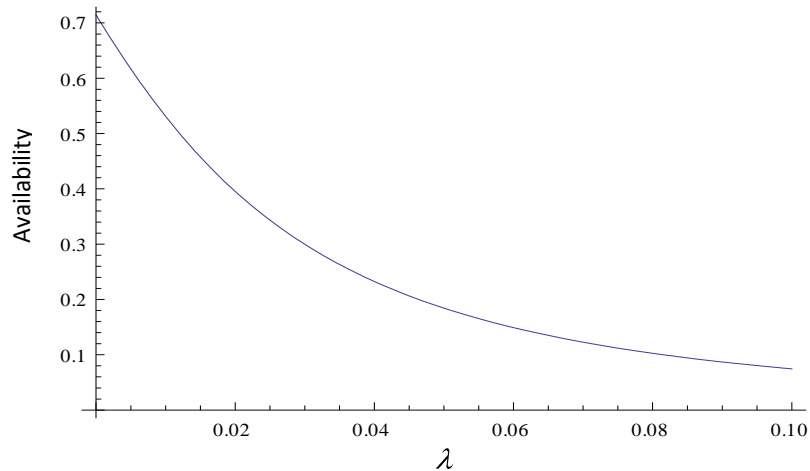


Figure 3. Availability versus failure rate λ .

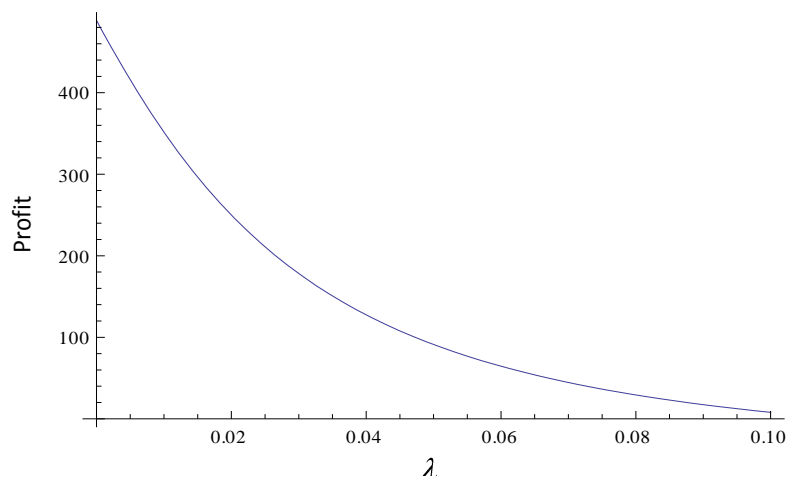


Figure 4. Profit versus failure rate λ .

The increase of failure rate λ at constant $\gamma=0.02$, $\alpha=0.04$, $\beta=0.06$, $\varphi=0.05$, $\tau=0.02$, $p=0.4$, $q=0.6$, $C_0=700$, $C_1=40$, $C_2=10$ the MTSF, Availability and PROFIT of the system decrease.

REFERENCES

- Goel LR, Gupta R, Singh SK (1985). "Profit analysis of a cold standby system with two repair distribution", *Microelectron. Reliab.* 25(3):467-472.
- Kumar A, Suresh KG, Gulshan T (1995). "Probabilistic analysis of a two-unit cold standby system with instructions at need". *Microelectron. Reliab.* 35(5):829-832.
- Kuo-Hsiung W, Wen-Lea P (2006). "Comparison of reliability and the availability between four systems with warm standby components and standby switching failure". *Appl. Math. Comput.* 28(21):17-21.
- Labib SW (1991). "Stochastic analysis of a two unit warm standby system with two switching devices". *Microelectron. Reliab.* 31(6):1163-1173.
- Mokaddis GS, EL-Sherbeny MS, Ayid YM (2009a). "Stochastic behavior of a two different systems with two-unit warm standby redundant system subject to random failure". *J. Math. Sci. Eng. Appl.* 3(1):329-338.
- Mokaddis GS, EL-Sherbeny MS, Ayid YM (2009b). "Stochastic behavior of a two-unit warm standby system with two types of repairmen and patience time". *J. Math. Stat.* 5(1):42-46.
- Pour DH, Singh JP (1996). "Stochastic behavior of a two unit cold standby redundant system subject to random failure". *Microelectron. Reliab.* 36(2):243-246.
- Singh RP, Taneja G, Siwach BS (2000). "Two unit warm standby system with accident and various types of repair". *J. Decis. Math. Sci.* 5-6(1-3):75-86.
- Sridharan V, Mohanavadivu P (1998). "Stochastic behavior of a two unit cold standby system with two type of repairman and patience time". *Math. Comput. Model.* 28(9):63-71.