

*Full Length Research Paper*

# Effects of different manufacturing methods on pharmaceutical properties and release kinetic models of ketoprofen sustained-release microparticles

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Extrusion-spheronization and the fluid bed method are valuable commonly applied methods in microparticle production. However, the characteristics of resultants prepared by these two methods have seldom been compared. The aim of this study was to investigate differences in pharmaceutical properties and release kinetics of sustained-release ketoprofen microparticles prepared by different manufacturing processes. Microparticles prepared by extrusion-spheronization displayed slower release rate resulting in increased diffusion path of the drug, a behavior distinct for microparticles with less Surelease<sup>®</sup>. The effects of manufacturing method on release rate was also significant for microparticles with less Surelease<sup>®</sup> compared to microparticles with more Surelease<sup>®</sup>. The release profiles of coated microparticles fitted well to the Higuchi's release model, but in cases of microparticles with larger Surelease<sup>®</sup> coating, the trend was towards a zero-order release model. These findings are valuable for comprehending the differences among different preparation processes and for choosing the optimal manufacturing method of sustained-release microparticles.

**Key words:** Ketoprofen, microparticles, sustained drug delivery, extrusion-spheronization, fluid-bed, dissolution release kinetics.

## INTRODUCTION

To improve efficiency and patient compliance, numerous oral sustained-release dosage forms are used in many therapeutic applications. Multiple-unit sustained-release dosage forms like microparticles are receiving greater attention due to advantages, such as flexibility during formulation development, that reduce batch-to-batch variability (Bodea and Leucuta, 1998; Ansel et al., 1999;

Bodea and Leucuta, 1997; Hamdani et al., 1996). Drug absorption is also enhanced via increased surface area than single-unit dosage forms, reduced risk of side effects by decreased possibility of dose-dumping associated with single-unit sustained release tablets, and reduced peak plasma fluctuations resulting in more stable drug absorption (Follonier and Doelker, 1992). Extrusion-spheronization and fluid bed method are the most commonly used techniques in micro-particulate drug delivery systems in the pharmaceutical industry because of advantages, which include convenience, reproducibility, and good control of process parameters (Esposito

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et al., 2000; Blanque et al., 1995; Gandhi et al., 1999; Tapia et al., 1993). Moreover, extrusion-spheronization and fluid bed technology are practical for high drug-load pellets and thus, are suitable for sustained-release dosage forms in which drug content is higher than conventional short-acting dosage forms (Hileman et al., 1993). Currently, their applications are not only in the pharmaceutical industry but in food and agriculture (Marmo, 2007; Jiménez-Aguilar et al., 2011).

Although different papers report on different preparation methods of sustained-released dosage forms, there has been no comparison of release-controlling characteristics of extrusion-spheronization and fluid bed method to date. The aim of this study was to compare the pharmaceutical properties and release kinetic models of different types of ketoprofen sustained-release formulations prepared by the two different methods. Ketoprofen, an effective non-steroidal anti-inflammatory and analgesic agent used to treat acute and chronic rheumatoid arthritis and osteoarthritis, was chosen as a suitable drug for investigation because of its short half-life (1 h) and irritating effects on gastric mucosa (Vergote et al., 2001; Hassan et al., 1995). Since pharmaceutical properties like elongation, particle size, and yield percentage of pellets prepared by extrusion-spheronization are influenced by complex process conditions, an L16 ( $2^{15}$ ) orthogonal array design was employed to investigate production and processing parameters affecting resultant microparticles and to determine the optimal formulation.

## MATERIALS AND METHODS

Ketoprofen powders were purchased from Wuxue Xunda Pharmaceutical Co. (China), while ketoprofen and fenoprofen were purchased from Sigma Chemical Co. (U.S.A.) and used as standard and internal standard for high performance liquid chromatography (HPLC) analyses, respectively. Comprigel<sup>®</sup> M102 (MCC) was purchased from Mingtai Chemical Co. (Taiwan) and Oruvail 200<sup>®</sup> from Brenntag Chemicals Co. (Taiwan). Non-pareil seeds (25-30#) (IPS. (srl.), Milano, Italy) and Surelease<sup>®</sup> (Colorcon, Japan) were used as supplied, while PVP K30 (Kollidon 30) were purchased from BASF Chemical Co. (Germany). All other chemicals were of analytic grade.

### Differential scanning calorimetry

Interactions between active ingredients and excipients were measured by differential scanning calorimetry (model DSC 7 Perkin-Elmer, U.S.A.). The physical mixtures of ketoprofen and excipients (MCC, PVP K30, Surelease<sup>®</sup>, starch, and talc) were dried in a vacuum oven at 40°C for 24 h to remove water from the samples. Each sample (6 mg) was placed in sealed flat-bottom aluminum sample pans and scanned from 50 to 300°C at a heating rate of 10°C/min. The microparticles prepared by different methods (F-S 50 and E-S 50) were grounded to powder form for DSC examination and the results were compared with individual DSC thermograms.

### Solubility test

Since ketoprofen is poorly soluble in acidic conditions, the addition

of surfactant may increase solubility and release rate for optimal bioavailability (Jinno et al., 2000; Vergote et al., 2002). In this study, a pre-formulatory study of different concentrations of surfactants on the equilibrium solubility of ketoprofen in different pH medium was conducted. For this, 0.1 g ketoprofen was added to 15 ml varying media (pH 1.2, 4.6, 6.8, and 7.4) of different surfactants (1% sodium lauryl sulfate or 5% PVP K30). The samples were placed on a shaker and agitated at 37°C, withdrawn at 6, 8, 10, 12, 24, 36, 48, and 72 h, and centrifuged at 10000 rpm. The supernatants were then analyzed by HPLC.

### Preparation of ketoprofen-loaded microparticles by extrusion-spheronization

The four main processing steps of extrusion-spheronization (E-N) method are blending, wet mixing, extrusion of wet mass into short cylinders, and spheronization of the extrudate using a spinning friction plate. Ketoprofen powder (40%) was previously mixed with PVP K30 (2%) and sodium lauryl sulfate (0.5%), which were added in the manufacturing process to improve the dissolution behavior, and excipients (MCC 50.5%, starch 5%, and talc 2%) for 5 min in a mixer (model KSMC50, Taiwan). The required amounts of water were then added to the dry blends and mixed for an additional 10 min to produce a wet mass, which was passed through an screw extruder (model SY-86070-4, Taiwan), the length of screen bores were 1.0 and 1.5 mm. The extrudate was processed in a spheronizer (model SY-86070-3, Taiwan), which consists of a rotating friction plate and spins at high speed at the bottom of cylindrical bowl, using different speeds for different spheronization times.

During the course of extrusion and spheronization, the microparticles properties were affected by different preparation situations. The characteristics of coated resultants were affected by pharmaceutical properties (e.g. elongation and particle size) of uncoated microparticles. To determine the effects of manufacturing processes and conditions on pharmaceutical properties of products and to obtain optimal manufacturing conditions, an L16 ( $2^{15}$ ) orthogonal array experimental design method was applied for an overall investigation. The experimental variables and design matrix were given in Tables 1 and 2. Six important variables in the manufacturing process - amount of water content (variable A), amount of binder (variable B), extrude speed (variable C), extrude screen size (variable D), spheronization speed (variable E), and spheronization time (variable F) - and three interactions (variable AxB, variable CxD, and variable ExF) were chosen to investigate the effect on elongation and yields of microparticles. Each variable occurred at two suitable levels (low level [1], high level [2]). For example, variable A represents amount of water content, low level and high level express 120 and 135 ml respectively (Table 1). In the first experiment (Run 1) as shown in Table 2, variables A, B, C and D are all low level, that is to say, 120 ml water and 1 g binder were used to make wet mass, then the wet mass was passed through an extruder of 1.0 mm screen size and the extrude speed was 30 rpm. The extrudate was processed in a spheronizer under 600 rpm for 5 min, and the resultant pellets were dried in a hot air oven and collected. In total, 16 experiments were performed in random order. The experimental results were analyzed with the design-expert<sup>®</sup> software (version 6) and data were compared statistically using analysis of variance (ANOVA) (Abdullah and Al-Khamis, 1993). According to the analyses earlier described, ketoprofen-loaded core microparticles (E-N) were prepared under optimal conditions and dried in a hot air oven at 40°C for further coating process.

### Preparation of ketoprofen-loaded microparticles by fluid bed method

Ketoprofen-loaded microparticles were prepared by coating

**Table 1.** Two levels of six variables in the experimental design.

Variables	Low level (1)	High level (2)
A: Amount of water content (ml)	120	135
B: Amount of binder (g)	1	4
C: Extrude speed (rpm)	30	60
D: Extrude screen (mm)	1	1.5
E: Spheronization speed (rpm)	600	1100
F: Spheronization time (min)	5	10

**Table 2.** Experimental design matrix of the L<sub>16</sub> (2<sup>15</sup>) orthogonal table.

Run	A	B	AxB	C	error	ExF	error	D	error	error	F	CxD	E	error	error
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
2	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2
3	1	1	1	2	2	2	2	1	1	1	1	2	2	2	2
4	1	1	1	2	2	2	2	2	2	2	2	1	1	1	1
5	1	2	2	1	1	2	2	1	1	2	2	1	1	2	2
6	1	2	2	1	1	2	2	2	2	1	1	2	2	1	1
7	1	2	2	2	2	1	1	1	1	2	2	2	2	1	1
8	1	2	2	2	2	1	1	2	2	1	1	1	1	2	2
9	2	1	2	1	2	1	2	1	2	1	2	1	2	1	2
10	2	1	2	1	2	1	2	2	1	2	1	2	1	2	1
11	2	1	2	2	1	2	1	1	2	1	2	2	1	2	1
12	2	1	2	2	1	2	1	2	1	2	1	1	2	1	2
13	2	2	1	1	2	2	1	1	2	2	1	1	2	2	1
14	2	2	1	1	2	2	1	2	1	1	2	2	1	1	2
15	2	2	1	2	1	1	2	1	2	2	1	2	1	1	2
16	2	2	1	2	1	1	2	2	1	1	2	1	2	2	1

ketoprofen solution onto non-pareil beads (25-30#) using a fluid-bed apparatus (model YC-FBDG-2, Taiwan). After PVP K30 (38 g) was dissolved in 1200 ml water, ketoprofen (200 g), talc (2 g), starch (5 g) and sodium lauryl sulfate (5 g) were added and the resultant dispersion was stirred completely and passed through a 200-mesh sieve. Subsequently, a pre-formulatory study was undertaken to obtain optimal processing conditions. The ketoprofen-loaded core microparticles were produced by spraying the dispersion on non-pareil seeds (25-30 #) using the following instrumental settings: feeding rate of the dispersion 10 rpm, inlet temperature of the drying air 30°C, and outlet temperature 45°C. The microparticles were collected and dried in a hot air oven at 40°C for further coating process.

#### Preparation of sustained-release ketoprofen microparticles

Surelease<sup>®</sup>, an aqueous dispersion of ethylcellulose and one of the most widely used water-insoluble coating polymers in sustained-release dosage forms, was chosen for its excellent physic-chemical stability, good flexibility, and minimum toxicity (Shailesh et al., 2010). To explore its influence on dissolution characteristics, different amounts of Surelease<sup>®</sup> (20 and 50 g) were diluted with water to make 60% w/w coating solution, which was sprayed on previously prepared microparticles (E-N and F-N) to obtain different sustained-release microparticles. Known weights of ketoprofen pellets (200 g) were transferred into a fluid bed apparatus with the following instrumental settings: feeding rate of

the dispersion 10 rpm, inlet temperature of the drying air 40°C, while the outlet temperature was 50°C. The uncoated (E-N and F-N) and coated (E-S 20, E-S 50, F-S 20, F-S 50) microparticles were collected and filled into 0# capsules for dissolutions studies. The amount of ketoprofen in the capsules was held constant at 200 mg, while the total weight varied (E-N, 500 mg; E-S 20, 520 mg; E-S 50, 550 mg; F-N, 450 mg; F-S 20, 470 mg; and F-S 50, 500 mg). The compositions of the different formulations were listed in Table 3.

#### Properties of ketoprofen sustained-release microparticles

##### Morphologic characterization of microparticles

The morphology of intact microparticles was investigated using both optical microscopy and scanning electron microscopy (model JSM 5300, Japan). An elongated character was selected to determine the shape of microparticles.

##### Elongation analysis

Pellet elongation was evaluated by optical microscopic imaging. The image analyzer is equipped with a computer system linked to a video camera and a microscope (magnification  $\times 40$ ). The elongation character was calculated as the max diameter ( $R_1$ ) divided by the min diameter ( $R_2$ ) of microparticles (Hellén and Yliruusi, 1993; Koo and Heng, 2001; Baert et al., 1993; Otsuka et

**Table 3.** The compositions of different formulations prepared by extrusion-spheronization and fluid-bed methods.

Formulations	E-N	E-S 20	E-S 50	F-N	F-S 20	F-S 50
Ketoprofen (g)	200	200	200	200	200	200
non-pareil beads (g)	-	-	-	200	200	200
MCC (g)	252.5	252.5	252.5	-	-	-
PVP K 30 (g)	10	10	10	38	38	38
Talc (g)	10	10	10	2	2	2
Starch (g)	25	25	25	5	5	5
Sodium lauryl sulfate (g)	2.5	2.5	2.5	5	5	5
Water (ml)	337.5	337.5	337.5	1200	1200	1200
Surelease® (g)	0	20	50	0	20	50

al., 1994) as shown in Equation 1. At least 70 microparticles for each sample were determined.

$$E = R_1 / R_2 \quad (1)$$

#### Size distribution of microparticles and yields analysis

The various batches were fractioned into eight particle size ranges using 1400, 1180, 1000, 850, 710, 600, and 425  $\mu\text{m}$  sieves on a moving sieve shaker (Retch Co., Ltd., Germany) for 15 min. The microparticles obtained from these various sieves were weighed and the yield (% w/w) was calculated as the weight of the most fraction microparticles obtained from size analysis distribution divided by the sum of the total weight of the microparticles.

#### Content uniformity of microparticles

To determine the amount of ketoprofen in the microparticles, the contents of different capsules were put in a flask and 100 ml methanol was added. The mixture was then sonicated. After centrifugation, the whole supernatant was collected and examined by photo-spectrometry at 254 nm.

#### Drug release studies

*In vitro* release profiles of microparticles prepared by different methods were compared with a commercially available formulation (Oruvial 200®). Dissolution studies were conducted using a standard USP XXIV dissolution apparatus with paddle method for different capsules. The temperature of the dissolution medium was maintained at  $37 \pm 0.5^\circ\text{C}$  and the rotation speed of the paddle was adjusted to 100 rpm. Capsules were introduced in 900 ml of pH 1.2 hydrochloride solution or pH 6.8 phosphate buffer medium. Subsequently, the samples (5 ml) were withdrawn at specific time intervals (10, 20, 30 min and 1, 2, 4, 6, 8, 10, 12, 14, 16, 18, 20, and 24 h) and analyzed by HPLC at 254 nm. The withdrawn samples were immediately replaced with fresh dissolution medium. All experiments were performed in triplicate. The dissolution characteristics were compared by using difference factors ( $f_1$ ) and similarity factor ( $f_2$ ), the two fit factors are defined by the equations (Polli et al., 1997; Goskonda et al., 1998):

$$f_1 = \frac{\sum_{t=1}^n |R_t - T_t|}{\sum R_t} \times 100\% \quad (2)$$

$$f_2 = 50 \log \left\{ \left[ 1 + \frac{1}{n} \sum_{t=1}^n (R_t - T_t)^2 \right]^{-0.5} \right\} \times 100 \quad (3)$$

Where  $n$  is the number of dissolution sample times,  $R_t$  and  $T_t$  are the cumulative percent released at each time point for the reference and test products, respectively. The  $f_1$  value was zero when the test and reference profiles were identical and increased proportionally with dissimilarity between the two profiles. On the other hand, the  $f_2$  value was 100 when the profiles were identical. An  $f_2$  value between 50 and 100 suggested that the two dissolution profiles were similar.

#### Dissolution release kinetics

To study the mechanism of drug release from different microparticles, drug release data were analyzed according to zero-order, first-order, Higuchi and Korsmeyer-Peppas model. The equations were described as follows (Higuchi, 1963; Korsmeyer et al., 1983; Costa and Sousa, 2001):

$$\text{Zero-order model: } Q_t = k_0 t \quad (4)$$

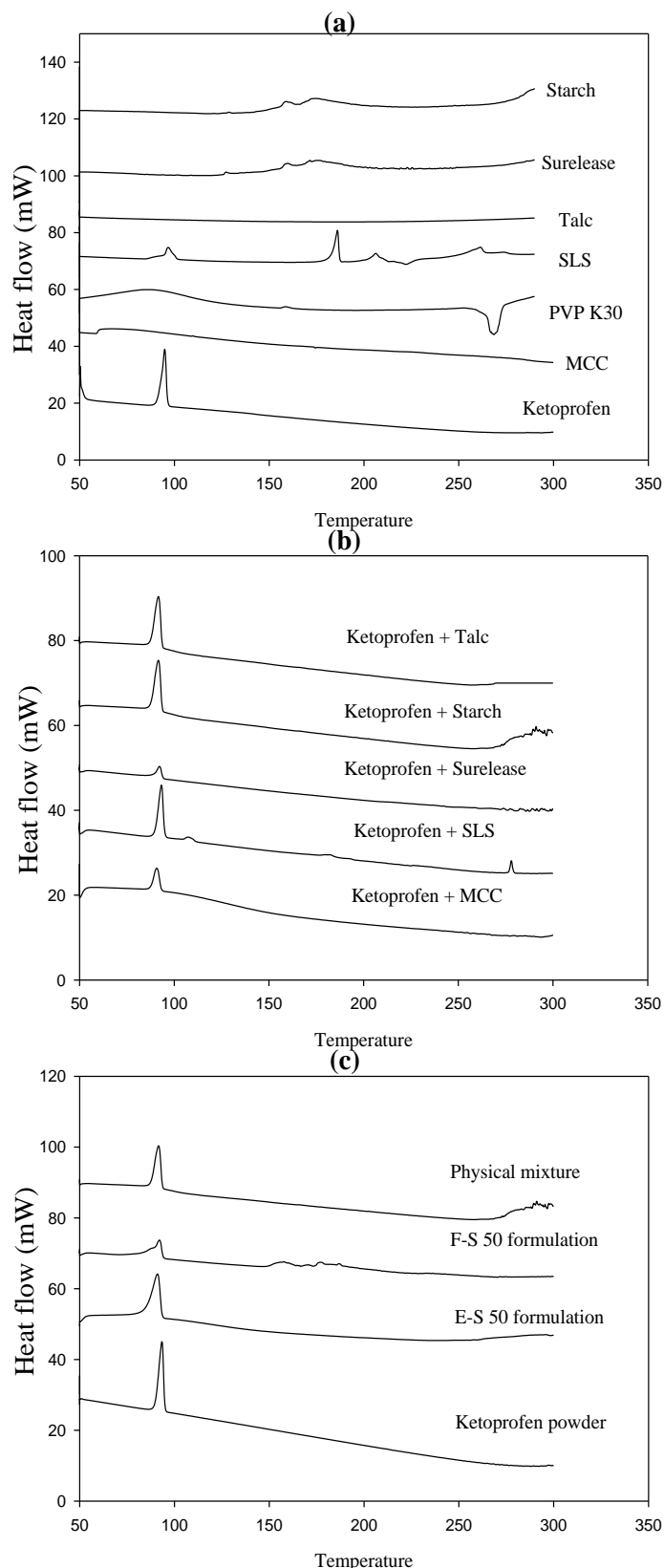
$$\text{First-order model: } \ln Q_t - \ln Q_0 = k_1 t \quad (5)$$

$$\text{Higuchi model: } Q_t = k_H t^{1/2} \quad (6)$$

Where  $Q_t$  is the amount of drug released at time  $t$ ,  $Q_0$  is the amount of drug released at time  $t = 0$ ,  $k_0$  is the zero order release constant,  $k_1$  is the first order release constant,  $k_H$  is the Higuchi release constant. Furthermore, to confirm the mechanism of drug release, the first 60% of drug release was fitted in Korsmeyer-Peppas model (Korsmeyer et al., 1983):

$$\text{Korsmeyer-Peppas model: } M_t / M_\infty = k t^n \quad (7)$$

Where  $M_t$  is the amount of drug released at time  $t$ ,  $M_\infty$  is the amount of drug release after infinite time,  $k$  is the rate constant and  $n$  is used to characterize different release mechanisms. In the case of a thin film, the  $n$  value for delivery systems in which drug release is primarily controlled by Fickian diffusion is 0.5 and for systems in which non-Fickian transport occurs,  $n$  will lie between 0.5 and 1.0, whereas  $n = 1$  to case-II transport (zero order release) (Lee, 1985). In the case of a cylinder and a spherical matrix, Fickian diffusion is predominant when  $n = 0.45$  and  $0.43$  instead of 0.5, and for Case II transport when  $n = 0.89$  and  $0.85$ , instead of 1.0 (Ritger and Peppas, 1987a, 1987b).



**Figure 1.** (a) DSC thermogram of ketoprofen and different excipients. (b) DSC thermogram of mixtures of ketoprofen and different excipients. (c) DSC thermogram of sustained release microparticles prepared by different methods (E-S 50 and F-S 50).

## RESULTS

### Differential scanning calorimetry (DSC)

Differential scanning calorimetry (DSC) was employed to explore the possible interaction between active ingredient (ketoprofen) and different excipients. The thermal curve of ketoprofen showed a sharp endothermic peak at 94°C (Figure 1a), which persisted at the thermogram of the mixture of ketoprofen and all excipients (MCC, PVP K30, Surelease®, starch, and talc) used in this study (Figure 1b). Moreover, the DSC thermogram of two microparticles prepared by different methods (F-S 50 and E-S 50) showed no appearance, shift, or disappearance of peak at 94°C (Figure 1c), which confirmed that ketoprofen deterioration did not occur during the manufacturing process and that the excipients used in this study were compatible with ketoprofen.

### Influence of surfactants and pH value of the dissolution medium on ketoprofen solubility

For the development of sustained-release dosage forms, drug solubility was one of the important factors to be considered, and the solubility profiles of ketoprofen in different pH media were shown in Figure 2. The comparison of profiles indicated that the solubility profile of ketoprofen was pH-dependent, such that it was poorly soluble in acidic conditions and that the solubility was increased by increasing the pH value of the medium. Since the solubility of ketoprofen in acidic medium was known to be relatively low, leading to a low dissolution behavior and low bioavailability, various methods have been used to improve the solubility (Ahn et al., 1998; Yamada et al., 2001) and one of the techniques was the incorporation of a small amount of surfactant (Vijaya Kumar et al., 2006). The addition of PVP K30 and SLS resulted in increased drug solubility in different pH media (Figure 2). Thus, surfactants were added during the pellet manufacturing process, resulting in sustained but complete release of ketoprofen.

### Experimental design of the preparation of ketoprofen-loaded microparticles

During the course of extrusion and spheronization, the microparticle properties were affected by different preparation situations. The variance between different formulations and the effective variables were explored by the L16 ( $2^{15}$ ) orthogonal experimental analyses. The results from a duplicate of the experiments are shown in Table 4. For the elongation analyses of microparticles, the important effects were the main effects of A and E, such that the amount of water content and spheronization speed were the two important effects that impacted on the elongation of micro particles. The response value of

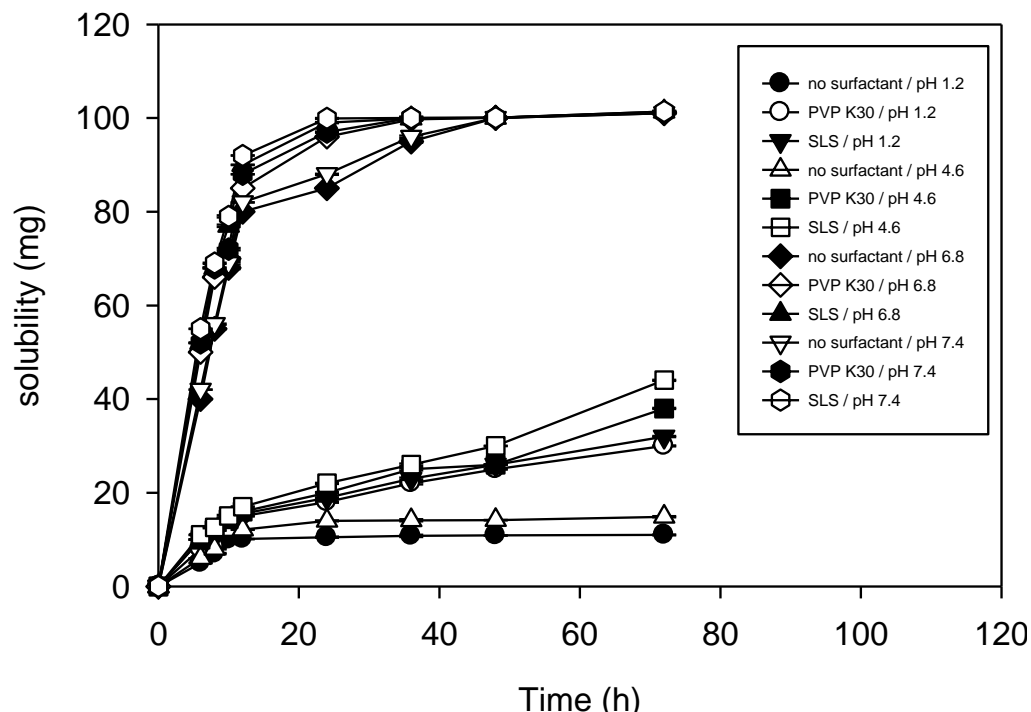


Figure 2. Solubility profile of ketoprofen with different surfactants in different dissolution media.

Table 4. Analysis of variance for elongation and yield percentage of pellets prepared by extrusion-spheronization.

Source of Variation	Degrees of Freedom	Elongation				Yield percentage			
		Sum of Squares	Mean square	F	prob>F <sup>b</sup>	Sum of Squares	Mean square	F	prob>F <sup>b</sup>
A	1	0.23	0.23	5.94*	0.0375	2040.33	2040.33	13.28*	0.0054
B	1	0.025	0.025	0.65	0.4400	950.80	950.80	6.19*	0.0346
C	1	2.40×10 <sup>-3</sup>	2.40×10 <sup>-3</sup>	0.062	0.8097	5.5	5.5	0.036	0.8542
D	1	7.89×10 <sup>-4</sup>	7.89×10 <sup>-4</sup>	0.020	0.8901	540.10	540.10	3.51	0.0936
E	1	0.63	0.63	16.16*	0.0030	14.25	14.25	0.093	0.7676
F	1	0.037	0.037	0.96	0.3539	11.12	11.12	0.072	0.7940
Residual	9	0.35	0.039	5.94*		1382.99	153.67		
Total	15	1.28		0.65		4945.80			

\*Significant; <sup>b</sup> $p < 0.0500$ .

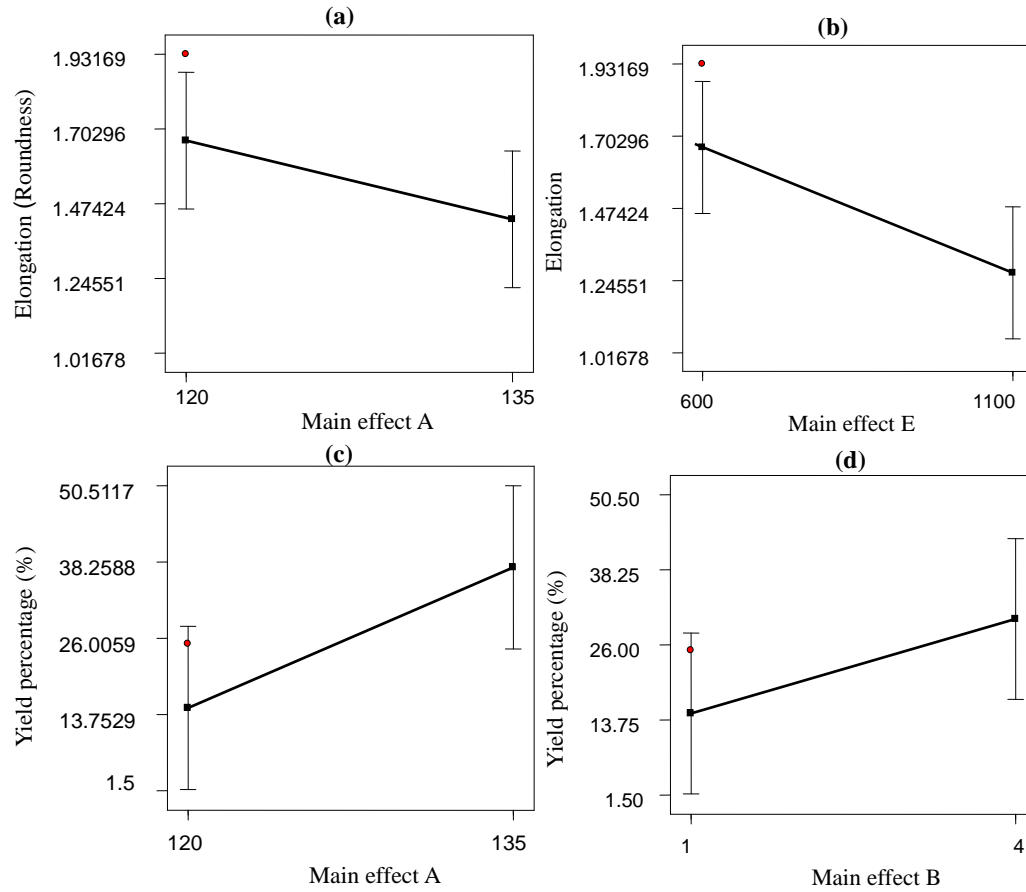
the effects showed that the effects of variables A and E were negative (Figure 3a and b). Increased variables A and E led to decreased elongation of microparticles and exhibited the best results arising from the low level of water content and spheronizing speed.

For the yield studies (Table 4), the important effects seemed to be variable A (amount of water content) and variable B (amount of binder). These two effects were positive for yield percentage and increasing them led to increased yields of microparticles (Figure 3c and d). According to the analyses aforementioned, in ketoprofen microparticles prepared under optimal conditions, the extrude speed, extrude screen size, and spheronization

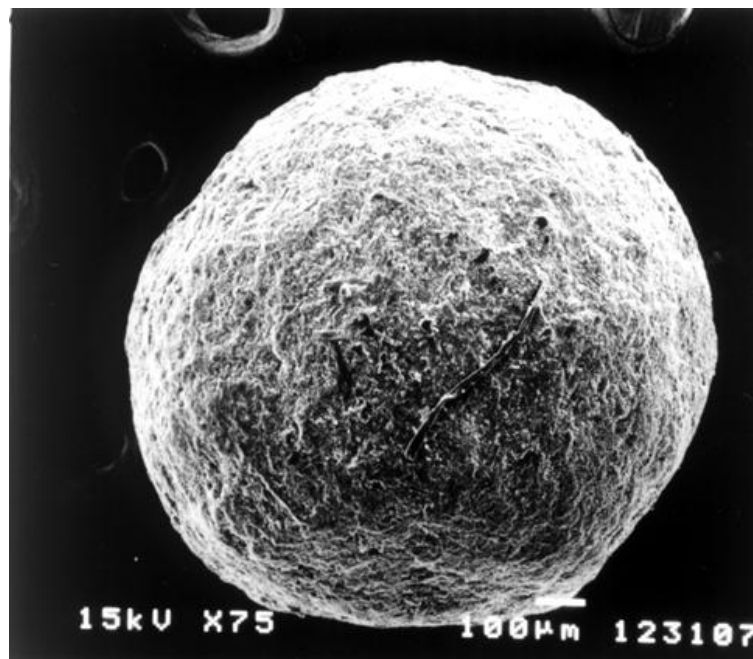
time did not have significant effects on the response studied. Thus, these variables could be fixed at convenient levels. The SEM photomicrograph of resultant microparticles showed a bit of roughness on the surface but fine elongation behavior (Figure 4).

#### Yield percentage and content uniformity of different formulations

The yield percentages of microparticles are shown in Table 5. Comparing the yield percentages of sustained-release microparticles prepared by different methods, the



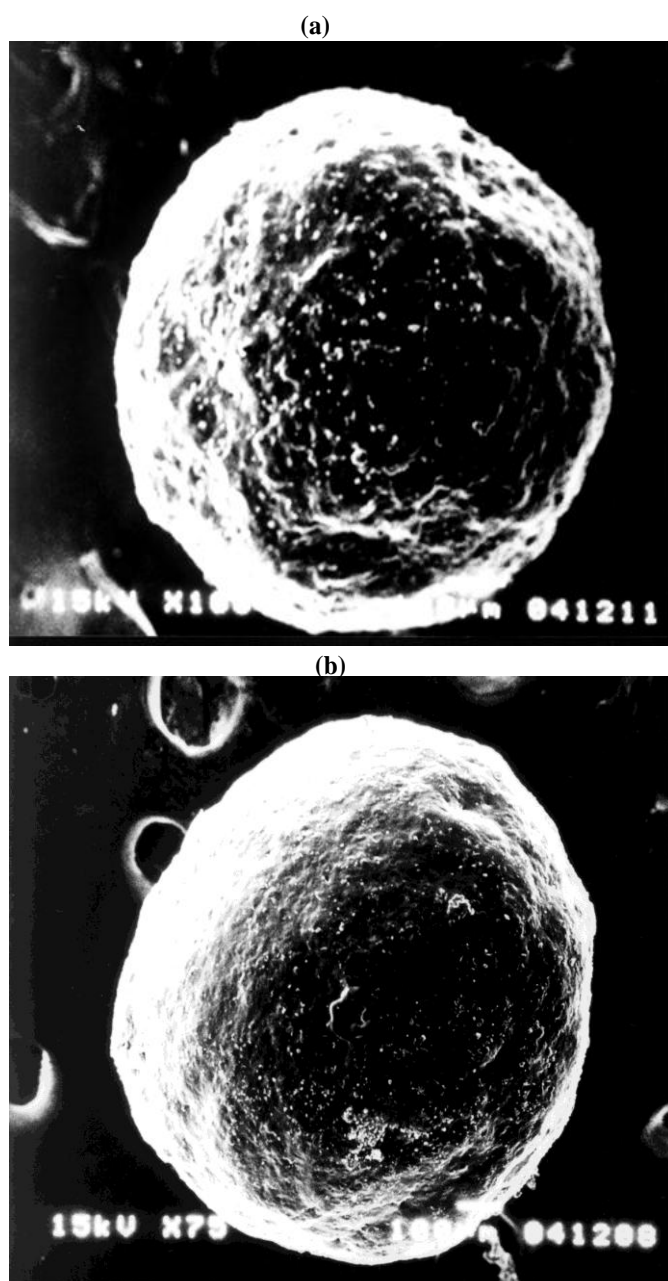
**Figure 3.** (a-b) Plots of elongation for water content (effect A) and spheronization speed (effect E), respectively. (c-d) Plots of yield percentage for water content (effect A) and amount of binder (effect B), respectively.



**Figure 4.** SEM photograph of E-N microparticles.

**Table 5.** Yield percentage and content uniformity of different formulations.

Formulation	Yield percentage (%)	content uniformity		
		Mean (%)	S.D	C.V. %
E-N	97.82	96.65	2.88	0.98
E-S 20	83.49	95.23	3.98	1.33
E-S 50	88.28	93.19	1.34	2.45
F-N	99.06	98.02	2.95	1.05
F-S 20	92.45	95.05	3.65	1.92
F-S 50	91.53	95.94	2.53	1.48

**Figure 5.** SEM photograph of (a) E-S 20 and (b) E-S 50 micro-particles.

yields of micro-particles prepared by the fluid bed method (F-S 20 and F-S 50) were higher than those of micro-particles prepared by the extrusion-spheronization method (E-S 20 and E-S 50). The contents of different micro-particles were between 93 to 98%, with less than 5% coefficient of variation (Table 5). There was no difference in terms of content uniformity of the resultant micro-particles among different manufacturing procedures.

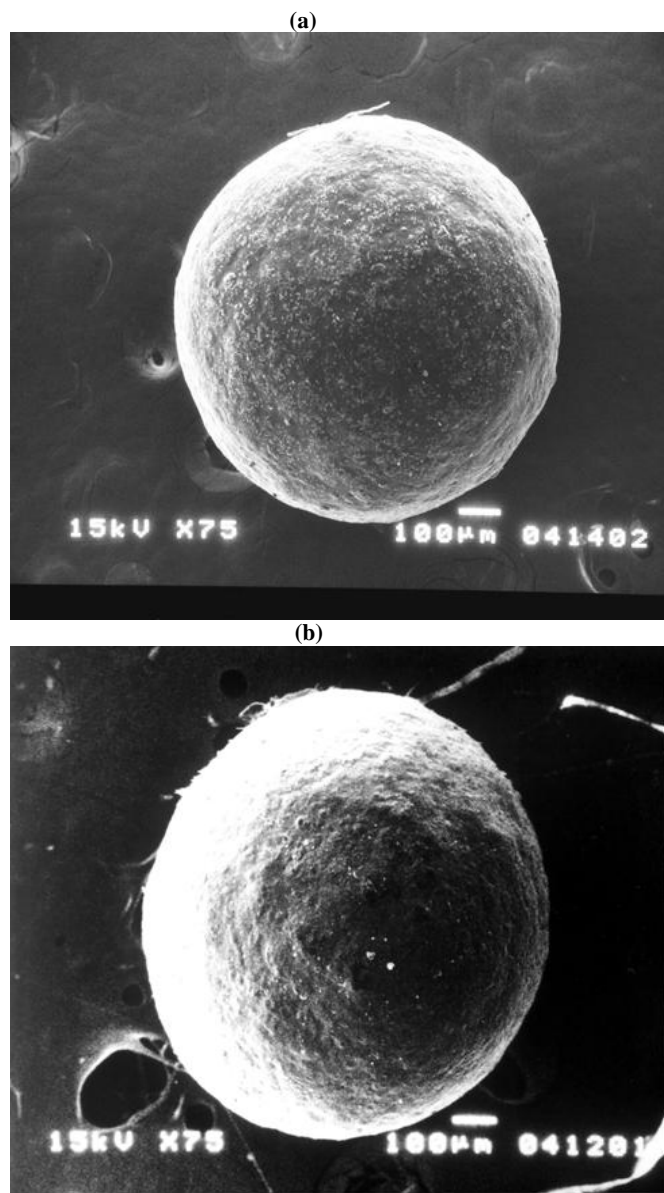
#### Morphological analysis of ketoprofen sustained-release micro-particles

The shape and surface of micro-particles prepared by extrusion-spheronization and fluid bed method with different amounts of Surelease<sup>®</sup> were examined using a scanning electron microscope (Figures 5 and 6). The surface of micro-particles prepared by the fluid bed method was smoother compared to that of micro-particles prepared by the extrusion-spheronization method. This might be because the surface of non-pareil seeds used by the fluid bed method was smoother than the uncoated micro-particle prepared by extrusion-spheronization, resulting in smoother surface of the resulting “coated micro-particles”. However, these surface phenomena were not related to drug release rates because ethylcellulose had high tensile strength (Piao et al., 2010).

#### Drug release for different micro-particles

The different amounts of Surelease<sup>®</sup> (20 and 50 g) used in the manufacturing processes were varied to investigate their effect on the drug release properties. The dissolution profiles obtained with the six formulations (E-N, E-S 20, E-S 50, F-N, F-S 20, F-S 50), as compared to Oruvail 200<sup>®</sup> commercial formulation in pH 1.2 and 6.8 conditions, are shown in Figure 7a and b. The release profiles from different formulation in pH 6.8 dissolution medium exhibited finer dissolution behavior than pH 1.2 dissolution medium, namely the effect of pH value of the dissolution medium on the release characteristics of ketoprofen was distinct. Comparing the release characteristics of different formulations under pH 1.2 dissolution

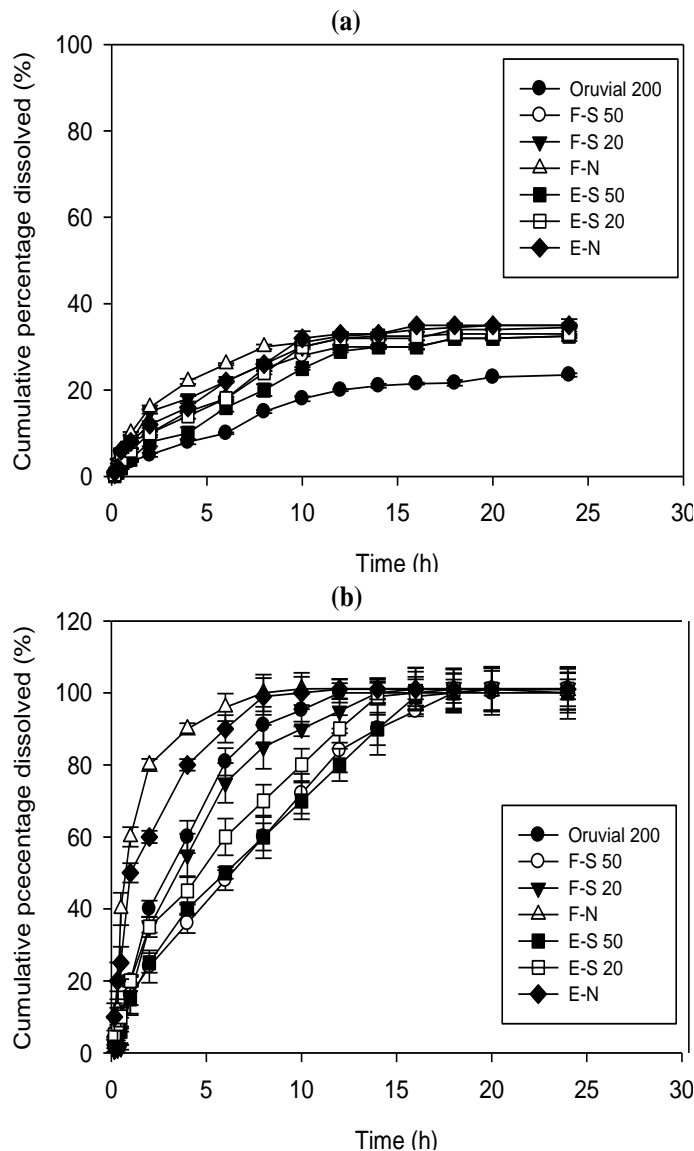




**Figure 6.** SEM photograph of (a) F-S 20 and (b) F-S 50 microparticles.

conditions, the dissolution profiles of six formulations were similar and very low, only nearly 30% of the total amount of ketoprofen released at 24 h after the start of the release test, while Oruvail 200<sup>®</sup> only had 20% released. This was identical to the results of the solubility test.

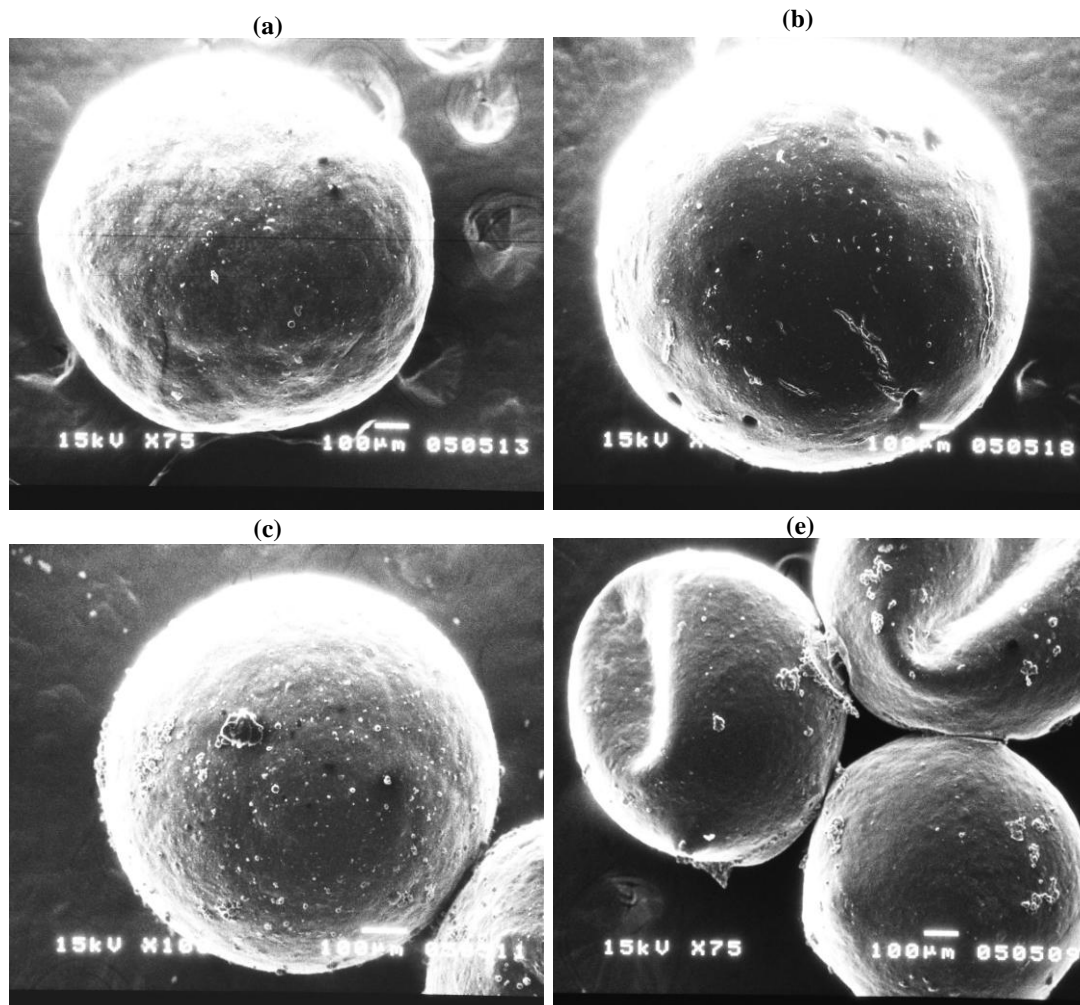
In pH 1.2 medium, the dissolution profiles of six formulations were similar and practically independent of composition and quantity of coating. The main limiting factor was very poor solubility of ketoprofen in acidic medium. The cause of the higher dissolution profiles of the six formulations compared to that of Oruvail 200<sup>®</sup> might be attributed to surfactants added in the manufacturing process. The diffusion and release properties



**Figure 7.** Release profile of different formulations and Oruvail 200<sup>®</sup> at (a) pH 1.2 and (b) pH 6.8 dissolution media. ● Oruvail 200<sup>®</sup>; ○ F-S 50; ▼ F-S 20; △ F-N; ■ E-S 50; □ E-S 20; ◆ E-N.

of insoluble active compounds were improved significantly to obtain enough solubility and release rate for the desired bioavailability (Li et al., 2006). On the other hand, in pH 6.8 dissolution medium, the micro-particles uncoated by Surelease<sup>®</sup> (F-N and E-N) exhibited fastest release rates. The E-S and F-N formulations dissolved rapidly and efficiently (around 60 and 80%, respectively, of the drug was released during the first 2 h), and the cumulative drug release percent could be increased to 100% within 8 and 12 h, respectively.

For other formulations, the following rank order concerning ketoprofen release rate was noted: F-N>E-N>F-S 20>E-S 20>Oruvail 200<sup>®</sup>>E-S 50 or F-S 50. The dissolution profiles of E-S 50 and F-S 50 exhibited faster kinetics in the first 1 h period, faster when the slope was



**Figure 8.** SEM photograph of microparticles after dissolution test (a) E-S 20, (b) E-S 50, (c) F-S 20, and (d) F-S 50.

reduced such that after 18 h, almost 100% of ketoprofen was dissolved. The release data were analyzed as per zero-order, first-order, Higuchi and Korsmeyer-Peppas models. The correlation coefficients ( $R^2$ ) of various kinetic models are given in Table 8. For all Surelease<sup>®</sup> coated formulations, the Higuchi square root model had the best fit with higher correlation ( $r^2 > 0.98$ ). When the release data were analyzed as Korsmeyer-Peppas equation, the  $n$  values of all formulations ranged between 0.53 - 0.84. The surface and morphology of microparticles after completing the release test in pH 6.8 medium were examined and the photomicrographs corresponding to E-S 20, E-S 50, F-S 20 and F-S 50 (Figure 8a to d, respectively) revealed that Surelease<sup>®</sup> was insoluble in water. The sunken surface was fabricated manually to show a hollow structure caused by the dissolution of ketoprofen and non-pareil seeds (Figure 8d). This might confirm that the release mechanism of coated microparticles was controlled by diffusion of the Surelease<sup>®</sup>

membrane.

## DISCUSSION

Comparing the pharmaceutical characteristics of resulting sustained-release microparticles, the results showed variances between microparticles prepared by different methods. Due to the narrow size distribution and preferable flow behavior of core microparticles prepared by the fluid bed method, these microparticles (F-S 20 and F-S 50) have higher yields than those prepared by extrusion-spheronization (E-S 20 and E-S 50). The core microparticles prepared by extrusion-spheronization are heavier, resulting in fewer amounts of microparticles to be blown up under the coating process and in reduced coating yield percentage. This phenomenon can be improved by increasing the quantity of core microparticles and by reducing the spraying flow rate. By increasing the

**Table 6.** Difference factors ( $f_1$ ) and similarity factor ( $f_2$ ) of microparticles prepared by different Surelease<sup>®</sup> amounts.

Formulations	pH 1.2		pH 6.8	
	$f_1$	$f_2$	$f_1$	$f_2$
E-N / F-N	7.296	56.983	7.378	55.935
E-S 20 / F-S 20	6.727	61.834	8.430	56.407
E-S 50 / F-S 50	7.554	56.682	2.622	81.612

**Table 7.** Difference factors ( $f_1$ ) and similarity factor ( $f_2$ ) of six formulations and Oruvail 200<sup>®</sup>.

Formulations	pH 1.2		pH 6.8	
	$f_1$	$f_2$	$f_1$	$f_2$
E-N	69.83	69.83	13.47	44.91
E-S 20	56.23	56.23	9.61	50.04
E-S 50	40.98	40.98	16.38	40.09
F-N	79.32	79.32	18.67	36.03
F-S 20	66.24	66.24	5.41	67.46
F-S 50	52.25	52.25	16.88	39.77

amount of Surelease<sup>®</sup>, the coating on microparticles surfaces has a remarkable effect in delaying the release of ketoprofen. This is obviously predictable such that an increase in the polymer proportion results in increased micro-particle coating layer and thus, in decreased drug diffusion and a reduction in drug release rate.

On the other hand, comparing the release characteristics of microparticles with the same amount of Surelease<sup>®</sup> but prepared by different procedures, microparticles prepared by extrusion-spheronization displayed a slower release rate. The release rate of E-S 20 was slower than that of F-S 20 and E-S 50 was slower than F-S 50. The possible reason may be the structural differences by the manufacturing processes. Ketoprofen are dispersed on the coating on the surface of non-pareil seeds for the fluid bed method, while ketoprofen are embedded in microparticles prepared by extrusion-spheronization. This phenomenon results in the increased drug diffusion path of microparticles prepared by extrusion-spheronization, and the reduced drug release rate, which is especially distinct for microparticles without Surelease<sup>®</sup> (E-S, F-S).

Based on the increase in Surelease<sup>®</sup>, the effect of diffused mechanism control by the coating membrane is more effective than the location of ketoprofen. Therefore, the release profiles of F-N 50 and E-N 50 formulations, which are coated by larger amounts of Surelease<sup>®</sup> and are almost identical, showed that the release rate is insignificantly affected by manufacturing process. Drug diffusion from the coating film is the main parameter affecting release rate. This correlation is confirmed using difference factors ( $f_1$ ) and similarity factor ( $f_2$ ) (Table 6). The  $f_1$  values range from 2.622 to 8.430 and the  $f_2$  value

between 55.935 and 81.612, suggesting that all of the formulations coated with same amount Surelease<sup>®</sup> showed similar release behavior, while the release profiles of E-S 50 and F-S 50 are almost the same because the  $f_1$  value approaches zero ( $f_1 = 2.622$ ) and the  $f_2$  value is nearly 100 ( $f_2 = 81.612$ ).

Furthermore, fit factors are also used to evaluate the difference between all formulations and commercial Oruvail 200<sup>®</sup> (Table 7). The release characteristic of all formulations is not similar for Oruvail 200<sup>®</sup> in pH 1.2 medium, whereas in pH 6.8 medium, the release characteristic of microparticles coated with 20 g Surelease<sup>®</sup> (E-S 20 and F-S 20) was similar to that of Oruvail 200<sup>®</sup>. In fact, F-S 20 has the most similar formulation because the  $f_1$  and  $f_2$  values are 5.41 and 67.46, respectively. The Higuchi square root model for all Surelease<sup>®</sup> coating formulations had the best fit with higher correlation ( $r^2 > 0.98$ ), which was commonly regarded as drug release following a diffusion-controlled mechanism (Korsmeyer et al., 1983; Wang et al., 2011). When the release data were analyzed as per Korsmeyer-Peppas equation, the  $n$  value was found in the range 0.62 - 0.82 with none and smaller Surelease<sup>®</sup> coated microparticles (E-N, F-N, E-S 20 and F-S 20), indicating non-Fickian diffusion as the mechanism from these microparticles. Whereas in the case of microparticles prepared with larger Surelease<sup>®</sup> (E-S 50 and F-S 50), the  $n$  value was in the range 0.83 - 0.85, indicating that the mechanism of drug release from formulation E-S 50 and F-S 50 were found to be close to zero order release kinetics. As shown in Figure 8b, it is obvious that the release kinetic model of E-S 50 and F-S 50 are near the zero-order model after 1 h of the release test, characterized by a constant slope of the release curve.

During the 1 and 12 h periods of the release profile, the values of the correlation coefficient are 0.9941 and 0.9994 for E-S 50 and F-S 50, respectively. The trend towards a zero-order release model of microparticles can be attributed to the larger Surelease<sup>®</sup> coating such that the release mechanism is controlled by the membrane independent of time (Yamada et al., 2001). The smaller Surelease<sup>®</sup> coated micro-particles exhibited as the Fickian or non-Fickian release mode was released by pure diffusion or diffusion coupled with erosion of a drug out of an encapsulating matrix (Lee, 1985; Ritger and Peppas, 1987a; Ritger and Peppas, 1987b; Wang et al., 2011). Therefore, it is feasible to modify the release rate and kinetic model by adjusting the coating amount of Surelease<sup>®</sup>. While the different manufacturing methods displayed different pharmaceutical characteristics and release rates, no influence was observed on release kinetics.

## Conclusion

The structural differences between microparticles manufactured by the extrusion-spheronization and fluid-bed

**Table 8.** *In vitro* release kinetics of ketoprofen from six microparticles and Oruvial 200®.

Formulations	pH 1.2					pH 6.8				
	Zero order	First order	Higuchi	Korsmeyer-Peppas		Zero order	First order	Higuchi	Korsmeyer-Peppas	
	R <sup>2</sup>	R <sup>2</sup>	R <sup>2</sup>	R <sup>2</sup>	n	R <sup>2</sup>	R <sup>2</sup>	R <sup>2</sup>	R <sup>2</sup>	n
Oruvial 200®	0.9559	0.5887	0.9914	0.9945	0.5694	0.9693	0.7553	0.9926	0.9867	0.8255
E-N	0.8838	0.6128	0.9777	0.9941	0.6322	0.8886	0.7639	0.9547	0.9656	0.7374
E-S 20	0.9793	0.6201	0.9957	0.9768	0.7067	0.9518	0.7829	0.9907	0.9889	0.8106
E-S 50	0.9632	0.6395	0.9912	0.9756	0.8418	0.9664	0.7397	0.9982	0.9842	0.8432
F-N	0.9224	0.5305	0.9898	0.9835	0.6169	0.9169	0.813	0.9361	0.9635	0.6888
F-S 20	0.8857	0.6137	0.9801	0.9549	0.6421	0.9655	0.7453	0.9805	0.9766	0.8207
F-S 50	0.9377	0.6306	0.9913	0.9737	0.8338	0.9749	0.7368	0.9947	0.9674	0.8471

methods resulted in different dissolution rates, while different Surelease® amounts resulted in different release kinetics. It is feasible to adjust the release characteristics by utilizing different operating conditions and ingredients, including surfactant and sustained-release materials. The findings obtained herein could be useful in understanding the release behavior differences and as guidelines for selecting processing methods in the preparation of sustained-release microparticles.

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