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Study of the roof behavior in longwall gob in long-term condition

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Assessment of the roof behavior in longwall gob and estimation of the occurrence of caving and fracturing zones above mined panels are the main factors used in evaluating abutment stresses, ground subsidence, face support and adjacent structures design. The combined height of caving and fracturing zones is taken as equivalent to the height of destressed zone (HDZ) in this study. The long-term estimation of this height plays a key role in accurate determination of maximum ground surface subsidence and the amount of transferred loads towards the neighboring solid sections. In this paper, the roof behavior in longwall gob has been studied in long-term condition. For this purpose, a time-dependent model based on the energy balance in longwall mining combined with a rheological model of caved materials with time-varying parameters was used to calculate HDZ. Also, parametric study was conducted to evaluate the effects of geometrical and geomechanical parameters on the roof caving and fracturing. Moreover, the calculated HDZ from the current study is compared with the results of the existing numerical, analytical and empirical models and the in-situ measurements reported in literatures. Comparative study confirms a good agreement that exists between the results of the present study with those of the in-situ measurements and empirical models. It can be concluded that the results of this research can be successfully used to evaluate HDZ in longwall gob in long-term condition to determine the induced stress and surface subsidence in longwall mining.

Key words: Longwall mining, height of destressed zone, time-dependent model, strain energy, rheological model.

INTRODUCTION

Longwall mining method is the most popular and high production method used for coal extraction in the world. This method is suitable for the extraction of relatively thick, slightly horizontal and uniform coal seams. The overall objective of coal mining is to obtain maximum productivity with reliable safety considerations. Besides that, mining efficiency exclusively depends on the stability of the gates, tunnels, pillars and stopes. The stability of these structures is also related to both the roof cave-in performance and the interaction of the caved materials with the roof rock strata. After extracting the coal seam and advancing the hydraulic jacks, the immediate roof of
the mined area collapses and caves into the void area behind the working face. The downward movement of the roof strata then gradually extends upwards and will cause the disturbed roof strata to become destressed. Thus, the overburden pressure above the destressed zone will be redistributed in the rock mass surrounding longwall panels directed to the front abutment and the two adjacent neighboring solid sections (Majdi and Rezaei, 2013; Rezaei et al., 2015a, 2015b, 2017; Rezaei, 2016, 2017).

There are common approaches for analyzing the fracturing and caving behavior of the panel roof rock strata including in-situ measurement and physical, empirical, numerical and analytical modeling. Although the in-situ tests and physical modeling provide useful and reliable results, they are time consuming and expensive (Rezaei et al., 2015a). On the other hand, empirical methods are based on the data extracted from a specific case study with particular characteristics and are not qualified for other cases with different mechanical or physical properties. Numerical modeling is widely used in this field particularly as a tool for assessing the caving progress. However, this method is time consuming and requires a large number of input variables which depend on the available data; this may need to be estimated or assumed. Thus several researchers have proposed mathematical methods to study the roof behavior over the mined panel in longwall mining.

Many researchers have investigated the behavior of roof rock strata, process of the gradual upward movement and determination of the height of caving and fracturing zones (Rezaei et al., 2017). According to these studies, it is concluded that there are zones of disturbance above the mined panel (Figure 1). These zones include caved, fractured and continuous deformation zones (Palchik, 2003). The extent of each zone depends on the geological and geomechanical properties of overburden strata including the strength characteristics of rocks, the in-situ stress, the thickness of coal seam, and overburden stress and the type and nature of the strata (Gao et al., 2014).

In the field of the current research topic, Rezaei (2016) and Rezaei et al. (2017) studied the roof caving and fracturing using the traditional and multilayer perceptron (MLP) artificial neural networks (ANNs), respectively. According to these studies, traditional and multilayer perceptron ANN models predict the height of destressed zone 3.1-86.5 and 2.4-81.64 times the extracted coal seam thickness, respectively. Sheng et al. (2017) applied the combination of borehole photography and the seismic CT scanner techniques to determine the height of caved and fractured zones over the longwall panel in a case study. Liu et al. (2017) studied the height of the water-flowing fractured zone based on the in-situ measurement,
mechanical theory calculation and numerical simulation. Wang et al. (2017) evaluated the separation and fracturing in the undermined overburden pressure using the theoretical and numerical models. They showed that theoretical model is suitable to quantify the extent of possible risk zones. Literature review in this field shows that there are many factors that can influence the roof strata behavior. These factors include coal seam characteristics, roof rock strata properties, stress conditions, etc (Le et al., 2017). However, all of these effective parameters were not simultaneously considered in the study of roof behavior in the previous investigations. An effort is made in the current study to overcome this limitation for improving the related results.

In order to study the roof behavior over the longwall panel in this study, the combination of the caving and fracturing zones is considered as the height of destressed zone (HDZ). Beyond this height, the induced stress due to the overburden depth will be transferred towards the adjacent solid sections. Therefore, height of destressed zone can play a vital role in the amount of transferrable stresses to front abutment, adjacent access tunnels, pillars and panel rib-sides. Accordingly, to suitably evaluate the amount of transferrable loads to the adjacent gates and the intervening pillars, the height of destressed zone must be estimated. The main objective of this paper is to study the roof behavior based on the determination of the HDZ over the longwall gob in long-term condition. The HDZ determination was conducted on the basis of the strain energy balance in longwall coal mining and a nonlinear rheological model of caved materials. In order to cover the available problems in previous researches, the effects of geometric parameters, roof rock strata strength properties, pressure time and temperature-dependent parameters of caved materials were considered in determining the height of destressed zone in this research.

**METHODOLOGY**

In this research, an extension model of the proposed one by Rezaei et al. (2015b) is used to study the roof behavior over the longwall gob in long-term condition. For this, the basic concept of energy consideration in longwall mining along with the calculation of the energy component in this area is discussed in detail.

**Basic conceptual model**

The concept of strain energy balance in longwall mining was firstly introduced and discussed by Rezaei et al. (2015a). In their opinion, longwall panel and its surrounding rock mass can be considered as a separate system in which the equilibrium between its energy components should be maintained. On this basis, as the extraction of coal seam from the panel starts in the longwall mining, the energy balance within the system enclosing the mine openings and surrounding rocks is distorted. However, energy balance must be preserved before and after the mining. A schematic configuration of longwall mining pre and post-mining is shown in Figure 2 in which states I and II are considered as the primary status and the end of coal (rock) extraction inside a panel, respectively (Rezaei et al., 2015a). In Figure 2, \( L_w \) is the panel width, \( H \) is the depth of cover, \( h_s \) is the extracted seam thickness, \( H_d \) is the depth of destressed zone, \( D \) is the distance of horizontal line across the centre of gravity of the panel to the ground surface, \( V_m \) is the volume of mined panel, \( S_m \) is the surface of mined panel, and \( V \) and \( S \) are the volume and surface of destressed zone above a panel.

![Figure 2. Longwall mining configuration: (a) before panel extraction or state I and (b) after complete extraction of a longwall panel or state II. Source: Rezaei et al. (2015a).](image-url)
mined rock (coal) is released and consumed in failing, caving and
destressing the panel roof rock strata (Rezaei et al., 2015a). This
process continues until the extraction of a longwall panel
completed. At the end of panel extraction and after the total
compression of caved materials, a defined zone with height of \( H_d \)
and the stored strain energy in
\( U_d \) is the stored strain energy in the mined rock (coal) and
\( U_c \) is the stored strain energy in caved rocks within the destressed
zone as given in Equation 1. Based on the stated equation, the height of
destressed zone (HDZ) was analytically determined in short-term
condition. The stored strain energy in the mined rock \( U_d \) is the
same in long and short-terms conditions but the stored strain
energy in the caved rocks within destressed zone \( U_d \) certainly is
different.

\[
U_m = U_d
\]  
(1)

where \( U_m \) is the stored strain energy in the mined rock (coal) and
\( U_d \) is the stored strain energy in the caved rocks within the
destressed zone.

Determining the stored strain energy in the mined area

For long-term calculation of the HDZ, the stored strain energy in the
extracted coal (rock) seam \( (U_m) \) and the stored strain energy in
the destressed zone \( (U_d) \) should be determined in long-term
conditions. The HDZ can be obtained by equating these two
mentioned energy components. Due to the complex conditions of
longwall mining, those general assumptions that considered by
Rezaei et al. (2015a) in calculating the involved energy components
are also regarded here. The difference between the long-term
calculation of HDZ in this research with the time-independent
energy model proposed by Rezaei et al. (2015a) is in the stored
strain energy within the destressed zone \( (U_d) \). Calculation of this
component is outlined in the following sub-section. However, the
stored strain energy in the extracted coal (rock) seam before any
extraction \( (U_m) \) is similar in short-term and long-term conditions
because mining is not started yet in both states. Therefore, the
equation developed by Rezaei et al. (2015a) is utilized here for
\( U_m \) calculation in this study:

\[
U_m = \left(1 + \nu \right) (1 - 2 \nu) \gamma A_m \sigma_v \left[ \frac{h_s^2}{3} + H^2 + H h_s \right]
\]  
(2)

where \( U_m \) is the stored strain energy in the extracted coal (rock)
seam, \( \sigma_v \) is the initial stress due to overburden pressure which is
equal to \( \gamma H h_s \), \( H \) is the depth of cover, \( \gamma \) is the panel roof rock's
average unit weight, \( h_s \) is the extracted coal (rock) seam
thickness, \( A_m \) is the cross section of the mined panel which is
equal to the panel width multiplied by the extracted coal seam
(rock) thickness \( (L_c \times h_s) \), \( \nu \) is the panel roof rock's average

\[
\text{Poisson ratio and } E \text{ is the panel roof rock's average elastic modulus.}
\]

Determining the stored strain energy in the destressed zone

The stored strain energy of caved materials within the destressed
zone \( (U_d) \) is generally composed of elastic \( (U_E) \) and viscoplastic
strain energies \( (U_V) \).

\[
U_d = U_E + U_V
\]  
(3)

Under pressure of the roof in long-term conditions, the mechanical
properties of the caved materials can change, so that the elastic
modulus and the coefficient of viscosity of caved materials also
change over the time. Thus, the viscoplastic strain energy of the
caved materials should be considered in calculations. In this
research, the rheological properties of the caved materials are
considered according to the nonlinear rheological constitutive
model established by Zhang et al. (2011). To investigate the
rheological properties of the caved materials in this model, elastic
modulus \( (E) \), coefficient of viscosity \( (\eta) \) and threshold value of
stress \( (\sigma_s) \) is considered based on the modified Bingham model
(Figure 3). Unlike previous models about the deformation of a
structure, the elastic modulus and the coefficient of viscosity are the
functions of time.

According to Zhang et al. (2011), the nonlinear rheological
constitutive model can be described as:

\[
\begin{align*}
\sigma &= E_0 \varepsilon^{a t} \varepsilon, \quad \sigma \leq \sigma_s \\
\sigma &= \frac{\varepsilon}{K} - \lambda \varepsilon, \quad \sigma > \sigma_s
\end{align*}
\]  
(4)

where \( \sigma \) is the stress of caved materials, \( \sigma_s \) is the threshold
value of stress, \( E_0 \) is the initial elastic modulus, \( a \) is the material
constant, \( t \) is the pressure time of caved materials, \( \varepsilon \) is the strain
of caved materials, \( \lambda \) is the slope of materials hardening stage
and \( K \) is the coefficient that is calculated by (Zhang et al., 2011):

\[
K = \frac{1}{E_0 \varepsilon^{-a t}} + \frac{t^a}{\eta_0 C_\alpha \sigma_s^a}
\]  
(5)

where \( \eta_0 \) is the initial coefficient of viscosity and; \( C, \mu \) and \( \alpha \)
are material coefficients related to temperature. Replacing
the \( B = 1/\eta_0 C_\alpha \) into Equation 5 leads to:

\[
K = \frac{1}{E_0 \varepsilon^{-a t}} + \frac{B t^a}{\sigma_s^a}
\]  
(6)

In Equation 4, the deformed caved materials have the viscoplastic
properties when \( \sigma \) approaches \( \sigma_s \). Therefore, the caved
materials system has the elastic properties when \( \sigma \leq \sigma_s \) and the

viscoplastic properties when $\sigma > \sigma_s$. Accordingly, the elastic and viscoplastic components of strain energy can be calculated based on its associated stress.

To calculate the elastic strain energy of the caved materials within the destressed zone, the common equation of strain energy is used. If the destressed zone above the longwall panel is considered as a separate system (surface with height of $H_d$ in Figure 2b), its absorbed elastic strain energy can be calculated as follows:

$$U_E = \frac{1}{2} \int \sigma \varepsilon \, dV = \frac{1}{2} \int_0^h \sigma \varepsilon \, Adh$$

where $\sigma$ is the applied stress on the caved materials, $\varepsilon$ is the strain occurring under the corresponding applied stress, $h$ is the height of the caved materials within the destressed zone and $A$ is the unit surface of the system. Here, $A_d$ is considered as the unit surface of destressed zone which is equal to the panel width multiplied by the unit length of longwall panel ($A_d = L_w \times 1^m$).

After the caving process is completed in which the caved materials are through compressed, no further caving will take place. This means that the caved materials are completely compacted and there is no void area for further roof caving. Therefore, the height of destressed zone will be constant and no increase. On this basis, released energy is consumed in the roof distressing with the height of $H_d$. Accordingly, it can be concluded that the total height of caved materials ($h$) can be equivalent to the height of destressed zone ($h = H_d$). By applying the aforementioned simplifications, Equation 7 is modified to:

$$U_E = \frac{1}{2} \sigma \varepsilon A_d H_d$$

The substitution of the elastic part of Equation 4 into Equation 8 leads to:

$$U_E = \frac{1}{2} E_0 e^{-\alpha t} A_d H_d e^2$$

In the aforementioned equation, $E_0$ is the initial elastic modulus which is taken as equivalent of elastic modulus ($E$) of the overburden rock mass. Thus, Equation 9 can be modified to:

$$U_E = \frac{1}{2} E e^{-\alpha t} A_d H_d e^2$$

The following equation can be used to describe the stress-strain behaviour of caved materials (Salamon, 1990):

$$U_E = \frac{1}{2} \frac{E}{E(t)}$$

Figure 3. Modified Bingham model.
Source: Zhang et al. (2011).
\[ \sigma_c = \frac{E_0 \varepsilon}{1 - \varepsilon / \varepsilon_m} \]  
(11)

where \( \sigma_c \) is the uniaxial compressive strength of caved materials, \( \varepsilon \) is the strain occurring under the applied stress, \( E_0 \) is the initial elastic modulus which is considered same elastic modulus of rock mass \( (E) \) and \( \varepsilon_m \) is the maximum possible strain of the bulked rock material.

From Equation 11, one can write:

\[ \varepsilon = \frac{\sigma_c}{E + \sigma_c \varepsilon_m} \]  
(12)

The following equation is used to show the relationship between the maximum strain \( (\varepsilon_m) \) and the bulking factor \( (b) \) (Yavuz, 2004):

\[ \varepsilon_m = \frac{b - 1}{b} \]  
(13)

Substituting Equation 13 for Equation 12 leads to:

\[ \varepsilon = \frac{\sigma_c}{E + \frac{b \sigma_c}{(b - 1)}} \]  
(14)

Now by substitution of Equation 14 for Equation 9, the elastic stored strain energy in caved materials within the destressed zone \( (U_d) \) is calculated as follows:

\[ U_E = \frac{E e^{-at} A_d H_d \sigma_c^2}{2[E + \frac{b \sigma_c}{(b - 1)}]^2} \]  
(15)

Similar method is applied to calculate the viscoplastic strain energy \( (U_V) \). The substitution of the viscoplastic part of Equation 4 for Equation 8 leads to:

\[ U_V = \left( \varepsilon^2 - \frac{\lambda \varepsilon^2}{2} \right) A H_d \]  
(16)

When Equation 14 substituted for Equation 16 and rearranged, the final equation of viscoplastic stored strain energy in caved materials within the destressed zone can be obtained:

\[ U_V = \frac{A_d H_d \sigma_c^2}{2[E + \frac{b \sigma_c}{(b - 1)}]^2} \left[ \frac{1}{K} - \lambda \right] \]  
(17)

Finally, the total stored strain energy in caved materials within the destressed zone \( (U_d) \) can be obtained by replacing Equations 17 and 15 with Equation 3 as follows:

\[ U_d = \frac{A_d H_d \sigma_c^2}{2[E + \frac{b \sigma_c}{(b - 1)}]^2} \left[ E e^{-at} + \frac{1}{K} - \lambda \right] \]  
(18)

Determining the height of destressed zone

According to Equation 1, the stored strain energy in the mined rock (coal) is equal to the stored strain energy in the caved materials within the destressed zone. Therefore, the substitution of Equations 18 and 2 for Equation 1 leads to the calculation of the height of the destressed zone \( (H_d) \) in long-term condition as follows:

\[ H_d = \frac{(1 + \nu)(1 - 2\nu) A_d \sigma_c}{(1 - \nu)E}\left[ \frac{h^2}{3} + H^2 + H h_s \right] \] \frac{A_d \sigma_c^2}{2[E + \frac{b \sigma_c}{(b - 1)}]^2} \left[ 2E e^{-at} + \frac{1}{K} - \lambda \right] \]  
(19)

All of the incorporated parameters in the aforementioned equation are defined previously.

RESULTS AND DISCUSSION

Results verification

To verify the outputs of the current study, obtained results are compared with the results of in-situ measurements conducted by other researchers (HaiHnt, et al., 2011; Zhimin et al., 2010; Rafiquislam et al., 2009) as well as with the results of analytical model proposed by Rezaei et al. (2015a) in short-term condition. It should be noted that the values of experimental coefficients shown in Table 1 are used in long-term condition calculations. Furthermore, the threshold value of stress \( (\sigma_d) \) is

<table>
<thead>
<tr>
<th>( \sigma_0 ) (MPa)</th>
<th>E (MPa)</th>
<th>B</th>
<th>( \mu )</th>
<th>( \alpha )</th>
<th>( \lambda )</th>
<th>a</th>
</tr>
</thead>
<tbody>
<tr>
<td>20</td>
<td>59</td>
<td>1.24</td>
<td>2</td>
<td>0.3</td>
<td>3</td>
<td>1</td>
</tr>
</tbody>
</table>

Source: Zhang et al. (2011).

Table 1. Experimental parameters used in plotting of the graphs.
assumed as the 80% of uniaxial compressive strength of caved materials and the pressure time of caved materials (t) is considered 1.5 years. The comparison results are shown in Table 2. As shown in Table 2, the resulted height of destressed zone long-term condition (current study) is in accordance with the results of in-situ measurement in dataset 3. Actually, the results of this study and in-situ measurements in dataset No. 3 are quite close together. However, the results of the current study are greater than the results of in-situ measurements in other two datasets. Also, the long-term condition results are too greater than the results in the short-term condition. This is due to the fact that the full compression of caved materials causes further fracturing and caving of the roof rock strata. Accordingly, the height of destressed zone can be increased during the time. On the contrary, in-situ measurements are usually conducted during the mining operations in which the full compression of caved materials is not occurred yet. Also, in short-term condition the effect of pressure time of caved material is ignored causing the height of destressed zone to be decreased compared to the long-term condition. Therefore, it can be concluded that the results of the current study can be consistent with reality in the long-term condition and consequently, these differences are reasonable to some extent.

### Table 2. Comparison of the results of suggested model with in-situ measurements.

<table>
<thead>
<tr>
<th>No.</th>
<th>Reference</th>
<th>H (m)</th>
<th>Lw (m)</th>
<th>Y (KN/m³)</th>
<th>E (GPa)</th>
<th>v</th>
<th>( \sigma_c ) (MPa)</th>
<th>b</th>
<th>( h_s ) (m)</th>
<th>( \text{In-situ} )</th>
<th>Short-term condition [4]</th>
<th>Long-term condition (Current paper)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>[14]</td>
<td>285</td>
<td>223</td>
<td>2.466</td>
<td>2.32</td>
<td>0.2775</td>
<td>31.3</td>
<td>1.5</td>
<td>4</td>
<td>51.7</td>
<td>47.72</td>
<td>77.81</td>
</tr>
<tr>
<td>2</td>
<td>[15]</td>
<td>253</td>
<td>200</td>
<td>2.6627</td>
<td>25.2</td>
<td>0.174</td>
<td>32.07</td>
<td>1.5</td>
<td>3.9</td>
<td>64.5</td>
<td>40.99</td>
<td>91.50</td>
</tr>
<tr>
<td>3</td>
<td>[16]</td>
<td>290</td>
<td>120</td>
<td>2.7</td>
<td>3.5</td>
<td>0.22</td>
<td>50</td>
<td>1.5</td>
<td>3.5</td>
<td>29.5</td>
<td>23.01</td>
<td>31.09</td>
</tr>
</tbody>
</table>

Rezaei et al. (2015a).

### Parametric study

Here, actual dataset No. 3 in Table 2 is applied to evaluate the effect of incorporated parameters on the HDZ. In this analysis, constant values of experimental parameters presented in Table 1 were utilized in the parametric study calculations. Similar to the previous sub-section, the threshold value of stress (\( \sigma_c \)) is considered as the 80% of uniaxial compressive strength of caved materials and the pressure time of caved materials (t) is considered 1.5 years in calculations. Accordingly, variation of the height of destressed zone over the longwall gob versus the extracted coal seam thickness is illustrated in Figures 4 and 5, respectively. In these figures, the rest of the parameters are kept constant according to actual data. Also, variations of extracted coal seam thickness and bulking factor are considered between 0 to 5 m and 1.05 to 1.8 (expansion factor 5 to 80%), respectively. Moreover, variations of the height of destressed zone versus the extracted coal seam thickness for different values of pressure time of caved material are as shown in Figures 6 to 11, respectively. In these figures, one of the parameters (chart target parameter) is changed and the rest are kept constant.

As shown in Figures 4 and 5, HDZ has direct and inverse relationships with extracted coal seam thickness and bulking factor, respectively. In Figure 5, the values of 1.05 and 1.8 are considered as the lower and upper limits of bulking factor, respectively. However, it can be concluded from this figure that variations of the height of destressed zone in bulking factors less than 1.1 (expansion factor less than 10%) is relatively high compared to the bulking factors more than 1.1. This result is in agreement with the result reported by Majdi et al. (2012) in which the average expansion factor of 5% and 10% was considered to represent the long-term and short-term conditions of the caved rocks in the goaf area, respectively.

In Figures 6 to 11, the effects of depth of cover, unit weight, elastic modulus, Poisson ration, uniaxial compressive strength pressure time of caved materials on the height of destressed zone are presented. In these figures, relationships between the height of destressed zone and extracted coal seam thickness are potted for different values of the aforementioned variables. For example, the relationships between HDZ and extracted coal seam thickness are as shown in Figure 6 for the different overburden depth. This figure shows that when the depth of cover
HDZ would increase, also increase. It can be seen from Figure 7 that HDZ is in direct relation with the panel roof rock's average unit weight. Figure 8 indicates that the higher average elastic modulus of panel roof rocks leads
Figure 6. Relationship between height of destressed zone and extracted coal seam thickness for different values of depth of cover.

Figure 7. Relationship between height of destressed zone and extracted coal seam thickness for different values of panel roof rock's average unit weight.
Figure 8. Relationship between height of destressed zone and extracted coal seam thickness for different values of panel roof rock's average elastic modulus.

Figure 9. Relationship between height of destressed zone and extracted coal seam thickness for different values of panel roof rock's average Poisson ratio.
Figure 10. Relationship between height of destressed zone and extracted coal seam thickness for different values of average uniaxial compressive strength of caved materials.

Figure 11. Relationship between height of destressed zone and extracted coal seam thickness for different values of pressure time of caved materials.
to the higher HDZ. It can be concluded from Figure 9 that as the panel roof rock’s average Poisson ratio increases, the HDZ would decrease. Figure 10 shows that the higher the uniaxial compressive strength of caved materials, the lower the HDZ. Finally, Figure 11 shows that HDZ increases by increasing the pressure time of caved materials.

The ratio between height of destressed zone and extracted coal seam thickness ($H_d/h_o$) resulted from this parametric study can be used as a basis for comparative analysis object with the previous methods in this field. Figure 4 shows as the extracted coal seam thickness varies from 0.5 to 5 m, the ratio of $H_d/h_o$ varies from 8.7 to 8.9. Similarly, it can be concluded from Figures 5 to 11 that the ratio of $H_d/h_o$ varies from 8.7 to 13.8, 2.9 to 78.1, 2.7 to 10.9, 3.9 to 12.4, 4.7 to 9.9, 8.8 to 32.7, and 4.11 to 33.1, respectively. According to the aforementioned analysis, the predicted HDZs in the current study are in the range of 2.7 to 78.1 times the extracted coal seam thickness (Table 3).

### Comparative analysis

In this section, the results obtained from the present study are compared with the comprehensive results of previous methods in this field (Majdi et al., 2012; Rezaei et al., 2015a; Rezaei 2016; Rezaei et al., 2017). Rounding up these literatures, there are numerous empirically and analytically relations as well as numerical, artificial neural network (ANN) and multivariate regression analysis (MVRA) models to estimate HDZ that were found in Rezaei (2016) and Rezaei et al. (2017). Accordingly, the summary results of the previous models in addition to the long-term calculation of HDZ as the coefficient of extracted coal seam thickness ($h_o$) are shown in Table 3. In this table, the results (HDZ) are described based on the coefficient of the extracted coal seam thickness ($h_o$). It can be concluded from this comparison that the lower limit of HDZ calculation in long-term condition is close to the lower limit of other methods especially in-situ measurements, empirical model and short-term calculation of HDZ. On the other hand, the upper limit of the HDZ calculation in long-term condition is close to the upper limit of empirical model, ANN model and in-situ measurements. Therefore, it can be concluded that the results of the current study are in close agreement with the in-situ measurements and other verified models as well. Furthermore, the most important advantage of the current study compared to the other analytical and empirical models is taking into account further effective parameters. In previous empirical and analytical models used to study the roof caving and fracturing behavior, only two parameters including extracted coal seam thickness and average bulking factor are utilized (Peng and Chiang, 1984; Majdi et al., 2012). Also, depth of cover and strength properties were incorporated in short-term prediction of HDZ by Rezaei et al. (2015a) besides two aforementioned parameters. In addition to the aforementioned parameters, the pressure time and temperature-dependent parameters of caved materials are considered in the present study.

Considering the aforementioned results, it is concluded that the results of the current study can be successfully used to study the roof caving and fracturing behavior over the gob in longwall mining. Beyond the calculated HDZ, the overburden weight will be transferred towards the front abutment and the two adjacent neighboring solid sections where the access tunnels, the intervening barrier pillars and the adjacent un-mined solid sections are located. In fact, the difference between the longwall depth ($H$) and the height of destressed zone ($H_d$) must be considered for the calculation of stress transfer towards the adjacent pillars and access tunnels. Another application of roof behavior study in long-term condition is to determine the maximum ground surface subsidence due to longwall mining. It is obvious that the maximum height of destressed zone in longwall mining obtained during the time while the height of destressed zone will be stable. Therefore, further caving is not accrued in the roof strata after the stabilization of the height of destressed zone. If the process of caving and fracturing is stopped and the height of destressed zone is fixed, then stress field of the system will return to its condition.

<table>
<thead>
<tr>
<th>Method of appraisal</th>
<th>HDZ ($\times h_o$)</th>
</tr>
</thead>
<tbody>
<tr>
<td>In-situ measurement</td>
<td>2-100</td>
</tr>
<tr>
<td>Empirical model</td>
<td>2-105</td>
</tr>
<tr>
<td>Analytical model</td>
<td>4.5-48</td>
</tr>
<tr>
<td>Numerical model</td>
<td>5.8-47.6</td>
</tr>
<tr>
<td>Short-term model</td>
<td>2.02-57.8</td>
</tr>
<tr>
<td>Artificial neural network model</td>
<td>2.4-86.5</td>
</tr>
<tr>
<td>Multivariate regression analysis model</td>
<td>10.02-40.93</td>
</tr>
<tr>
<td>Long-term model (current study)</td>
<td>2.7-78.1</td>
</tr>
</tbody>
</table>
before the mining operations. Accordingly, stress transfer to the neighboring solid sections does not occur, nor does additional subsidence takes place in the ground surface.

Conclusion

In the present research, the roof caving and fracturing behaviors are studied in long-term condition. The conducted theoretical calculations were based on the strain energy balance during the longwall mining along with a constitutive rheological model of caved materials with time-varying parameters. Parametric study was also performed to evaluate the effect of influencing parameters on the HDZ. The results showed that depth of cover, panel roof rock's average unit weight, extracted coal seam thickness, panel roof rock's average elastic modulus and pressure time of caved materials have direct relationships with the HDZ. On the contrary, average uniaxial compressive strength of caved materials, panel roof rock's average Poisson ratio and bulking factor of caved materials have inverse relationships with it. To verify the current study results, calculated HDZ were compared with the results of available previous models as well as with in-situ measurements proposed by other researchers. The comparative conclusions have proved that the results of this study are in close agreement with the results of in-situ measurements and with the other comparable methods. The general significance of this study is that it incorporates the effects of geometric parameters, roof rock strata properties and pressure time and temperature dependent parameters of caved materials in roof behavior analysis. The long-term evaluation of roof rock strata behavior plays an important role in accurate estimation of transferred loads towards the gates and pillars. In fact, the difference between longwall depth and HDZ must be taken into account in calculation of stress transfer towards the front abutment and the adjacent ribsides. Furthermore, estimation of this height can help to determine the maximum ground surface subsidence due to longwall mining.

CONFLICT OF INTERESTS

The authors have not declared any conflict of interests.

REFERENCES


