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# Factors that affect pressure distribution of horizontal wells in a layered reservoir with simultaneous gas cap and bottom water drive

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Understanding the behaviour of pressure distribution completed in two layered reservoir subject to both active gas cap and bottom water drive mechanisms is very important in reservoir management. To determine the factors that affect pressure distribution of horizontal wells in a layered reservoir subjected simultaneously with a gas-cap at the top and bottom water drives, well completion was carried out in a particular layer and one of the parameters was varied while the others were kept constant. The results show that the following factors: (i) Wellbore radius (ii) Well Length and (iii) Pay thickness affect pressure distribution in two-layered reservoir subject to both active gas cap and bottom water drive which affect pressure distribution.

Key words: Well, pressure, layer, reservoir, well.

#### INTRODUCTION

A lot of work has been done on pressure distribution for both vertical well and wells (Abbaszadeh and Hegeman, 1990; Kuchuk et al., 1991; Owolabi et al., 2012; Clonts and Ramey Jr., 1986), however, much work has not been done on this subject we are considering in this paper. A good knowledge of effect of well parameters on pressure distribution of horizontal wells in a layered reservoir subject to simultaneous top gas-cap and bottom water drive is an important tool in reservoir management in the production of oil and gas (Ozkan and Raghavan, 1990; Oloro et al., 2013) hence it became an urgent need for this study to be carried out. In this study, the effect of the following factors on pressure distribution on horizontal wells in a two-layered reservoir which is being subjected simultaneously with gas cap and bottom water drive were considered: (i) Wellbore radius (ii) Well Length and (iii) Pay thickness. In determining the effect of these factors, a model that was developed previously in my paper titled "Pressure distribution of horizontal wells in a layered reservoir with simultaneous gas cap and bottom water

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Figure 1. Two-layered reservoir system containing horizontal wells.

LD1	LD2	ZWD1	ZWD2	ZD1	ZD2	DZ (ft)
0.19764	0.194	0.995	0.788	0.005	0.004	2.5
h <sub>D1</sub>	h <sub>D2</sub>	X <sub>wD1</sub>	XwD2	YeD1	YeD2	DX (ft)
4.785	2.5298	0.99244	0.795	0.0015	0.0215	2.00E+02
XeD2	XeD1	K2 (Md)	Kx2 (Md)	k1 (mD)	kx1 (mD)	Dy (ft)
0.0215	0.14	10	10	8.94427	10	21
Ct₁ (psi-1)	ct₂ (psi⁻¹)	L1 (ft)	L2 (ft)	h1 (ft)	h2 (ft)	
4.00E-06	3.00E-06	250	250	200	100	
YD1	YD2	Ø1	Ø2	YWD1	YWD2	
8.00E-03	6.00E-03	0.23	0.23	9.92E-01	8.94E-01	
XD1	XD2	µ1 (cp)	µ2 (cp)	hD2	hd1	
0.00757	0.0065	0.5	0.2	2.5298	4.785	

drive" was used (Oloro et al., 2013).

derivation are in Oloro et al. (2013).

#### METHODOLOGY

Pressure distribution of horizontal wells in layered reservoir with active top gas cap and bottom water drives models were used to determine effect of well parameters on pressure distribution (Oloro et al., 2013). This was done by varying a particular parameter which we want to know the effect on the pressure distribution and keeping other parameters constant.

The model diagram is shown in Figure 1 and model equation is given in Oloro et al. (2013). Reservoir and well properties are shown in Table 1. The derivation of Equations 1 and 2 are given in Appendices A and B (Oloro et al., 2013).

#### Model description and mathematical model for Layer 1

A physical description of the problem illustrated in Figure 1, is two layered reservoir, bounded on top by gas cap at the bottom by bottom water drive. A horizontal well of length L (along the x-axis), width  $y_w$  (along the y-axis) and stand-off  $z_w$  (along the z-axis) is drilled at the centre. The models used in this work and the

#### **RESULTS AND DISCUSSION**

To determine the effect of wellbore radius on wellbore pressure in Layer 1,  $P_{wD1}$  was computed for  $r_{WD1}$  values of  $1.14 \times 10^{-1}$  and  $4 \times 10^{-2}$ , while keeping other parameters constant. The results are presented in Table 2 and also illustrated in Figure 2 on log-log axes. It is observed from the figure that at early  $t_{D}$ , there is an obvious change in  $P_{wD1}$  with change in  $r_{wD1}$ . The change in  $P_{wD1}$  at later  $t_{D}$  is not obvious as it is shown in Figure 2.

Effect of change in wellbore radius of Layer 1 on pressure distribution for Layer 2 after radial flow period are presented in Table 3 and Figure 3. Results show slightly high productivity when smaller wellbore radius is used.

Effect of change in wellbore radius of Layer 1 on pressure distribution on Layer 2 at wellbore are presented in Table 4 and Figure 4. It is observed that a change in wellbore radius of Layer 1 does not have effect on  $P_{wD2}$ . Effect of change in  $r_{wD1}$  on  $P_{wD2}$  after

t <sub>D</sub>	P <sub>wD1</sub> (rwD1=1.14E-1)	P <sub>wD1</sub> (rwD1=4E-2)
0.001	3.170692	7.6770781
0.01	20.9151	24.860549
0.1	38.6595	42.04402
1	56.40391	59.227491
10	74.14832	76.410962
100	91.89272	93.59443
1000	109.6371	110.7779

**Table 2.** Effect of change in wellbore radius of Layer 1 on pressure distribution on Layer 1 at wellbore.



Figure 2. Effect of change in wellbore radius of Layer 1 on pressure distribution on Layer 1 at wellbore.

t <sub>D</sub>	P <sub>D2</sub> (rwD1=1.14E-1)	P <sub>D2</sub> (rwD1=4E-2)
0.001	7.79E+00	7.82E+00
0.01	2.49E+01	2.50E+01
0.1	4.22E+01	4.23E+01
1	5.94E+01	5.95E+01
10	7.67E+01	7.70E+01
100	9.41E+01	9.49E+01
1000	1.13E+02	1.13E+02
10000	1.13E+02	1.13E+02
1.00E+03 1.00E+02 PD2 1.00E+01 1.00E+00		PD2(rwD1=1.14E-1) PD2(rwD1=4.E-2)
1	10 100 1000 10000	

Table 3. Effect of change in wellbore radius of Layer 1 on pressure distribution for Layer 2 after radial flow period.

Figure 3. Effect of change in wellbore radius of Layer 1 on pressure distribution for Layer 1 after radial flow period.

radial flow period is shown in Figure 4.

Effect of change in wellbore radius of Layer 1 on pressure distribution for Layer 2 after radial flow period is shown in Table 5 and Figure 5.

It was observed that a change in  $r_{wD1}$  after radial flow period does have effect on  $P_{wD2}$ . Effect of change in  $r_{wD2}$ on  $P_{wD1}$  is shown in Table 5. It is observed that at early  $t_{D}$ ,  $P_{wD1}$  is higher for smaller wellbore radius, but at late

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t <sub>D</sub>	P <sub>wD2</sub> (rwD1=1.14E-1)	P <sub>wD2</sub> (rwD1=4E-2)
0.001	7.6770781	7.6770781
0.01	24.860549	24.860549
0.1	42.04402	42.04402
1	59.227491	59.227491
10	76.410962	76.410962
100	93.59443	93.594432
1000	110.7779	110.7779

Table 4. Effect of change in wellbore radius of Layer 1 on pressure distribution on Layer 2 at wellbore.



Figure 4. Effect of change in wellbore radius of Layer 1 on pressure distribution on Layer 2 at wellbore.

t <sub>D</sub>	P <sub>D2</sub> (rwD1=1.14E-1)	P <sub>D2</sub> (rwD1=4E-2)
0.001	7.79E+00	7.82E+00
0.01	2.49E+01	2.50E+01
0.1	4.22E+01	4.23E+01
1	5.94E+01	5.95E+01
10	7.67E+01	7.70E+01
100	9.41E+01	9.49E+01
1000	1.13E+02	1.13E+02
10000	1.13E+02	1.13E+02

Table 5. Effect of change in wellbore radius of Layer 1 on pressure distribution for Layer 2 after radial flow period.



Figure 5. Effect of change in wellbore radius of Layer 1 on pressure distribution for Layer 2 after radial flow period.

t <sub>D</sub>	P <sub>wD1</sub> (rwD2=0.032)	P <sub>wD1</sub> (rwD2=0.0312)
0.001	3.170692	0.110955
0.01	20.9151	17.85536
0.1	38.6595	35.59977
1	56.40391	53.34417
10	74.14832	71.08858
100	91.89272	88.83298
1000	109.6371	106.5774

Table 6. Effect of change in wellbore radius of Layer 2 on pressure distribution on Layer 1 at wellbore.



Figure 6. Effect of change in wellbore radius of Layer 2 on pressure distribution on Layer 1 at wellbore.

Table 7. Effect of change in wellbore radius of Layer 2 on pressure distribution on Layer 2 after radial flow period.

t <sub>D</sub>	P <sub>wD2</sub> (rwD2=0.03	32)	P <sub>wD2</sub> (rwD2=0.0312)
0.001	7.2992004		7.6770781
0.01	24.482671		24.860549
0.1	41.666142		42.04402
1	58.849613		59.227491
10	76.033084		76.410962
100	93.216555		93.594432
1000	110.40003		110.7779
1000 100 PwD2 10			→ PwD2(rwD2-0.032) → PwD2(rwD2-0.0312)
1		<b>1000</b>	

Figure 7. Effect of change in wellbore radius of Layer 2 on pressure distribution on Layer 2 after radial flow period.

 $t_{\text{D}}$  the effect of change in  $r_{\text{wD2}}$  is not much as shown in Figure 5.

Effect of change in wellbore radius of Layer 2 on  $P_{wD2}$ after radial flow period is shown in Table 6 and Figure 6. The effect is clearly seen in the table. It is observed that the larger the wellbore radius the higher the productivity in Layer 1.

Effect of change in wellbore radius of Layer 2 on pressure distribution in Layer 2 after radial flow period is shown in Table 7 and Figure 7. The effect is clearly

t <sub>D</sub>	P <sub>WD1</sub> (L <sub>D1</sub> =0.129764)	P <sub>WD1</sub> (L <sub>D2</sub> =4XI <sub>D1</sub> )	P <sub>WD1</sub> (L <sub>D3</sub> =39.53L <sub>D1</sub> )
0.001	19.29772	4.726915	0.488160695
0.01	37.04212	9.07335	0.937028341
0.1	54.78653	13.41979	1.385895988
1	72.53094	17.76622	1.8347636
10	90.27534	22.11266	2.28363128

Table 8. Effect of change in well length of Layer 1 on pressure distribution on Layer 1 at wellbore.

Table 9. Effect of change in well length of Layer1 on pressure distribution on Layer 2 at wellbore.

t <sub>D</sub>	P <sub>wD2</sub> (L <sub>D1</sub> =0.129764)	P <sub>wD2</sub> (L <sub>D2</sub> =4XL <sub>D1</sub> )	P <sub>wD2</sub> (L <sub>D3</sub> =6.18X L <sub>D1</sub> )
0.001	21.938443	21.93844299	21.93844299
0.01	39.121914	39.12191384	39.12191384
0.1	56.305385	56.3053846	56.30538468
1	73.488856	73.48885552	73.48885552
10	90.672326	90.67232	90.67232637

Table 10. Effect of change in well length of Layer 1 on pressure distribution on Layer 1 after radial flow period.

t <sub>D</sub>	P <sub>D1</sub> (L <sub>D1</sub> =0.12964)	P <sub>D1</sub> (L <sub>D2</sub> =0.52964)	P <sub>D1</sub> (L <sub>D1</sub> =0.802964)
0.001	2.26E+01	2.62E+01	2.66E+01
0.01	39.6309	46.4733	47.2315
0.1	56.6558	66.2005	67.2544
1	73.691	85.2431	86.517
10	90.7309	100.82	101.933

Table 11. Effect of change in well length of Layer 1 on pressure distribution on Layer 2 after radial flow period.

t <sub>D</sub>	P <sub>D2</sub> (L <sub>D1</sub> =0.12964)	P <sub>D2</sub> (L <sub>D1</sub> =0.52964)	P <sub>D2</sub> (L <sub>D1</sub> =0.802964)
0.001	2.20E+01	2.23E+01	2.23E+01
0.01	3.92E+01	3.98E+01	4.02E+01
0.1	5.64E+01	5.79E+01	5.96E+01
1	7.35E+01	7.62E+01	7.98E+01
10	9.07E+01	9.83E+01	1.08E+02

seen in Table 7. It is observed that the smaller the wellbore radius the higher the productivity.

To determine the effect of change in  $L_{D1}$  on  $P_{wD1}$ ,  $P_{WD1}$  was computed at values of  $L_{D1}$ , 0.12964, 0.529764 and 5.129764. The results are shown in Table 8. It is observed that the smaller the  $L_{D1}$  the larger the  $P_{wD1}$ .

Effect of change in  $L_{D1}$  on  $P_{wD2}$  is as shown in Table 9. The results show that change in  $L_{D1}$  does not affect  $P_{wD2}$ . Effect of change in  $L_{D1}$  on  $P_{D1}$  after radial flow period is shown in Table 10. The results show that the larger the  $L_{D1}$  the larger the  $P_{D1}$ . Effect of change in  $L_{D1}$  on  $P_{D2}$  after radial flow period is shown in Table 11. From the table, it is observed that the larger the  $L_{D1}$ , the larger  $P_{D2}$ .

Effect of change in  $L_{D2}$  on  $P_{wD1}$  is shown in Table 12. It is observed that change in  $L_{D2}$  does have effect on  $P_{wD1}$  as shown in Table 12.

Table 13 present the results of effect of change in well length of Layer 2 on pressure distribution on Layer 2 at wellbore. From the results, it was observed that the smaller the well length the higher the productivity of Layer 2 at wellbore and also after radial flow period as

t <sub>D</sub>	P <sub>wD1</sub> (L <sub>D2</sub> =0.134)	P <sub>wD1</sub> (L <sub>D2</sub> =0.334)	P <sub>wD1</sub> (L <sub>D2</sub> =0.534)
0.001	9.57E+00	1.00E+01	5.70E+00
0.01	26.5751	9.07947	9.07343
0.1	43.531	24.7054	14.2927
1	60.4684	31.9553	18.5834
10	77.1985	38.4888	22.8478
100	93.4722	42.8425	27.0495

Table 12. Effect of change in well length of Layer 2 on pressure distribution on Layer 1 at wellbore.

Table 13. Effect of change in well length of Layer 2 on pressure distribution on Layer 2 at wellbore.

t <sub>D</sub>	PwD2 (LD2=0.134)	PwD2 (LD2=0.334)	PwD2 (LD2=0.534)
0.001	21.93844	8.806508	5.505152361
0.01	39.1219	15.695618	9.817109
0.1	56.30538468	22.589585	14.12906657
1	73.4888555	29.483553	18.44102367
10	90.6723	36.37752	22.75298077
100	107.8557972	43.271488	27.06493

Table 14. Effect of change in well length of Layer 2 on pressure distribution on Layer 2 after radial flow period.

t <sub>D</sub>	P <sub>D2</sub> (L <sub>D2</sub> =0.134)	P <sub>D2</sub> (L <sub>D2</sub> =0.334)	P <sub>D2</sub> (L <sub>D2</sub> =0.534)
0.001	7.82E+00	8.88E+00	5.52E+00
0.01	2.50E+01	1.57E+01	9.82E+00
0.1	4.23E+01	2.29E+01	1.42E+01
1	5.95E+01	3.01E+01	1.85E+01
10	7.70E+01	3.64E+01	2.28E+01
100	9.49E+01	4.80E+01	2.72E+01

 Table 15. Effect of change in pay thickness of Layer 1 on pressure distribution on Layer 1.

Td	P <sub>wD1</sub> (h <sub>D1</sub> =4.785)	P <sub>wD1</sub> (h <sub>D1</sub> =8.785)	P <sub>wD1</sub> (h <sub>D1</sub> =15.785)
0.001	11.98235	21.9989	39.527
0.01	23	42.227	75.874
0.1	34.02	62.455	112.22
1	45.03596	82.6835	148.5669
10	56.0538	102.9117	184.91
100	67.072	123.14	221.26
1000	78	143.368	257.61
10000	89.107	163.5964	293.95

shown in Table 13.

Effect of change in well length of Layer 2 on pressure distribution on Layer 2 after radial flow period is shown in Table 14. The result shows that the small the well length in Layer 2 higher the productivity in Layer 2. To determine the effect of change in  $h_{D1}$  on  $P_{D1}$  and  $P_{D2}$ ,  $P_{D1}$  and  $P_{D2}$  were computed with values of  $h_{D1}$  of 4.785, 8.785 and 15.785. While  $h_{D2}$  remain constant at 6.5298. The results are shown in Tables 15 and 16. From these tables it is observed that a change in  $h_{D1}$ 

Td	P <sub>wD2</sub> (h <sub>D1</sub> =4.785)	P <sub>wD2</sub> (h <sub>D1</sub> =8.785)	P <sub>wD2</sub> (h <sub>D1</sub> =15.785)
0.001	19.196	19.195988	19.195988
0.01	34.23	34.2314	34.2314
0.1	49.27	49.266828	49.266828
1	64.30224	64.3022	64.3022
10	79.3376	79.337	79.337
100	94.37	94.37	94.37
1000	109.4085	109.4085	109.4085
10000	124.444	124.4439	124.4439

Table 16. Effect of change in pay thickness on of Layer 1 on pressure distribution on Layer 2.

Table 17. Effect of change in pay thickness of Layer 2 on pressure distribution on Layer 2.

Td	P <sub>wD2</sub> (h <sub>D1</sub> =4.785)	P <sub>wD2</sub> (h <sub>D1</sub> =8.785)	P <sub>wD2</sub> (h <sub>D1</sub> =15.785)
0.001	19.196	19.195988	19.195988
0.01	34.23	34.2314	34.2314
0.1	49.27	49.266828	49.266828
1	64.30224	64.3022	64.3022
10	79.3376	79.337	79.337
100	94.37	94.37	94.37
1000	109.4085	109.4085	109.4085
10000	124.444	124.4439	124.4439

Table 18. Effect of change in pay thickness of Layer 2 on pressure distribution on Layer 2.

t <sub>D</sub>	P <sub>wD2</sub> (h <sub>D2</sub> =6.5298)	P <sub>wD2</sub> (h <sub>D2</sub> =8.5298)	P <sub>wD2</sub> (h <sub>D2</sub> =10.5298)
0.001	19.195988	19.195988	30.955
0.01	34.2314	44.72	55.2
0.1	49.266828	64.3566	79.45
1	64.3022	83.997	103.69
10	79.337	103.6378	127.938
100	94.37	123.2784	152.184
1000	109.4085	142.92	176.43
10000	124.4439	162.5596	200.675

does affect only  $P_{D1}$  and not  $P_{D2}$ .

Also to determine effect of  $h_{D2}$  on  $P_{D2}$ ,  $P_{D2}$  were computed with values of  $h_{D2}$  at 6.5298, 8.5298 and 10.5298, while  $h_{D1}$  remain constant at 4.785. The results are shown in Table 18. This implies that to obtain high productivity for a particular layer the well should be positioned at a higher pay thickness.

#### Conclusions

From the statement of problems, objectives, and the results of study presented in the previous chapters, the

following conclusions can be drawn:

(1) It is possible to analyze each layer.

(2) When there is crossflow, pressure transient in the reservoir considered is similar to the behavior of the homogeneous system.

(3) Gas cap drive is more predominant than that of water drive.

(4) Well eccentricity was not found to affect productivities.

(5) Well location further away from the top and bottom boundaries offer delayed in external fluid breakthrough for all well completions. (6) The thicker the pay thickness of a particular layer the higher the wellbore pressure.

(7) In order to obtain high productivity, smaller wellbore radius should be used in Layer 1 and larger wellbore radius should be used in Layer 2.

(8) The longer the well length of a particular layer the higher the wellbore pressure.

#### Nomenclature

- C<sub>t</sub>: Total reservoir compressibility (Psi<sup>-1</sup>)
- h: Formation thickness (ft)
- h<sub>D</sub>: Dimensionless height
- L<sub>D</sub>: Dimensionless length
- P<sub>D</sub>: Dimensionless pressure
- P<sub>wD</sub>: Dimensionless wellbore pressure
- p<sub>D</sub>: Dimensionless pressure derivative
- S: Instantaneous source functions
- t: Time (h)
- t<sub>D</sub>: Dimensionless time
- x,y,z: Space coordinates
- x<sub>D</sub>,y<sub>D</sub>: Dimensionless distance in the x and y directions
- x<sub>f</sub>: Horizontal well half length
- z<sub>D</sub>: Dimension distance in the z director
- k: Horizontal permeability
- $k_v$  Permeability in the y direction (md)
- k<sub>z</sub>: Permeability in the z direction (md)
- I: Horizontal well length (ft)
- r<sub>D</sub>: Dimensionless radial distance in the horizontal plane
- r<sub>wD</sub>: Dimensionless wellbore radius
- $x_w$ : Well location in the x direction (ft)
- x<sub>e</sub>: Distance to the boundary or reservoir length (ft)
- x<sub>eD</sub>: Dimensionless distance to the boundary
- x<sub>WD</sub>: Dimensionless well location in the x- direction
- Z<sub>w</sub>: Well location in the direction (ft)
- z<sub>WD</sub>: Dimensionless well location in the Z direction
- Y<sub>w</sub>: Well location in the y direction (ft) Dimensionless well location in the Y direction.

#### **Conflict of Interest**

The author(s) have not declared any conflict of interests.

#### REFERENCES

- Abbaszadeh M, Hegeman PS (1990). Pressure-transient analysis for a slanted well in a reservoir with vertical pressure support. SPE Form. Eval. 5(3):277-284.
- Clonts MD, Ramey Jr. HJ (1986). Pressure Transient Analysis for wells with Horizontal Drainholes. SPE Paper presented at the 56<sup>th</sup> California Regional Meeting of the Society of Petroleum Engineers, Oakland, C.A, April 2-4.
- Kuchuk FJ, Goode PA, Wilkinson DJ, Thambynayagam RKM (1991). Pressure-transient behavior of horizontal wells with and without gas cap or aquifer. SPE Form. Eval. 6(1):86-94.
- Oloro J, Adewole SE, OlafuyiOA (2013). Pressure Distribution Of Horizontal Wells In A Layered Reservoir With Simultaneous Gas Cap And Bottom Water Drive." Am. J. Eng. Res. (Accepted for publication).
- Owolabi AF, Olafuyi OA, Adewole ES (2012). Pressure distribution in a layered Reservoir with gas-cap and bottom water. Nig. J. Technol. (NIJOTECH) 31(2):189-198.
- Ozkan E, Raghavan R (1990). Performance of horizontal wells subject to bottomwater drive. SPE Reserv. Eng. 5(03):375-383.